

# **Assessment of wind and wave data measured at IJmuiden Munitiestortplaats**

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## Acknowledgement

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## Summary

As part of the We@Sea project “Operation and Maintenance Cost Estimator” (OMCE) the 3-hour average wave and the 3-hour average wind data published by Rijkswaterstaat for the location “IJmuiden Munitiestortplaats” in the following denoted as YM6 have been analysed. Data measured over the period January 1990 - December 2001 have been considered. The coordinates of YM6 are 52°33’00” east and 4°03’30” north, and the water depth is 21 m. Besides the results over a period of 12 years also the four yearly seasons are considered separately, where these seasons are defined as follows:

- Winter : December, January, February;
- Spring : March, April, May,
- Summer : June, July, August;
- Autumn : September, October, November

To calculate the revenue losses due to downtime the capacity factor of the wind turbine has to be determined. For this purpose the wind speed distribution at YM6 is described by a 2-parameter Weibull distribution. Generally this Weibull distribution is based on 10-minute average wind speed data. However, 3-hour average data are available only so that the Weibull parameters of the wind speed distribution are based on these 3-hour average data. Although the parameters presented here are less accurate, they are still suitable to estimate the capacity factors and subsequently the revenue losses.

*Weibull parameters of average wind speed distribution at YM6*

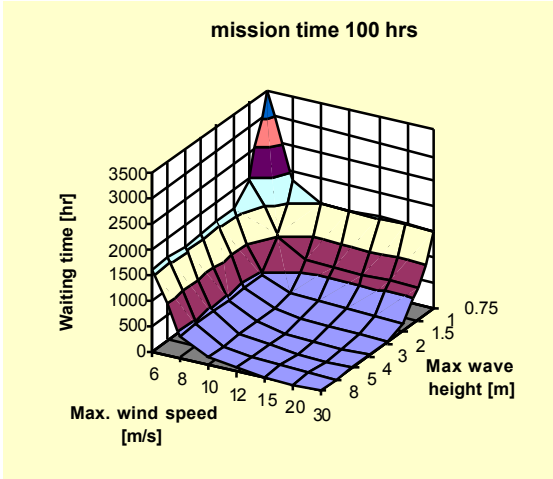
|                       | Winter | Spring | Summer | Autumn | Year |
|-----------------------|--------|--------|--------|--------|------|
| shape parameter       | 2.16   | 2.27   | 2.29   | 2.16   | 2.16 |
| scale parameter       | 8.90   | 7.41   | 6.98   | 8.07   | 7.84 |
| mean wind speed [m/s] | 7.88   | 6.57   | 6.18   | 7.15   | 6.94 |

The downtime of a wind turbine after a failure or the Time To Repair (TTR) is of importance to estimate different types of costs, f.i. the revenue losses and it appears that especially the waiting time due to bad weather conditions ( $T_{wait}$ ) is of great importance for the total downtime. During this period an access system may be available but is not allowed to leave the harbour. The capabilities of an access system are particularly dependent on the weather window in which it can be operated. The weather window of an access system is characterized by the maximum significant wave height  $H_{s,max}$  and the maximum wind speed  $V_{w,max}$  during which a certain maintenance action can be performed. Besides the weather window the duration is of importance. For the weather windows specified in the table below the waiting time has been calculated as function of the duration of the mission, and the results are presented as 3rd order polynomials. The coefficients of these polynomials are presented in this report.

*Overview of weather windows*

| Weather window number | $H_{s,max}$<br>[m] | $V_{w,max}$<br>[m/s] | Weather window number | $H_{s,max}$<br>[m] | $V_{w,max}$<br>[m/s] |
|-----------------------|--------------------|----------------------|-----------------------|--------------------|----------------------|
| 1                     | 0.75               | 6                    | 16                    | 2                  | 15                   |
| 2                     | 0.75               | 8                    | 17                    | 3                  | 8                    |
| 3                     | 0.75               | 10                   | 18                    | 3                  | 10                   |
| 4                     | 1                  | 6                    | 19                    | 3                  | 12                   |
| 5                     | 1                  | 8                    | 20                    | 3                  | 15                   |
| 6                     | 1                  | 10                   | 21                    | 3                  | 20                   |
| 7                     | 1                  | 12                   | 22                    | 4                  | 12                   |
| 8                     | 1.5                | 6                    | 23                    | 4                  | 15                   |
| 9                     | 1.5                | 8                    | 24                    | 4                  | 20                   |
| 10                    | 1.5                | 10                   | 25                    | 4                  | 30                   |
| 11                    | 1.5                | 12                   | 26                    | 5                  | 15                   |
| 12                    | 2                  | 6                    | 27                    | 5                  | 20                   |
| 13                    | 2                  | 8                    | 28                    | 5                  | 30                   |
| 14                    | 2                  | 10                   | 29                    | 8                  | 20                   |
| 15                    | 2                  | 12                   | 30                    | 8                  | 30                   |

The characteristic behaviour of the waiting time is shown in the figure below, where the waiting time is presented as function of the weather windows considered, viz. as function of the maximum allowable significant wave height and the maximum allowable wind speed.



*Waiting time as function of the maximum allowable wave height and the maximum allowable wind speed*

Logically the waiting time decreases when the weather windows become less harsh. It appears that this decrease is most significant for wave heights up to 1,5 - 2 m and wind speeds up to 10 - 12 m/s. So using access systems that can operate up to wave heights of 2 m and wind speeds up to 12 m/s will have a strong positive effect on the down time. On the other hand it is questionable whether an investment in access systems that can operate at wave heights above 2 m and at wind speeds above 12 m/s should be made for this location with these conditions. In general the advantage in terms of waiting time is only limited. However depending on the number of times and the duration a device is needed it might be advantageous in specific situations.

# 1. Introduction

## 1.1 Operation and Maintenance Cost Estimator

It is well known that the O&M costs of an offshore wind farm contribute to the total exploitation costs significantly [1]. The objective of the We@Sea project “Operation and Maintenance Cost Estimator” (OMCE) is to determine a methodology with which owners and operators of offshore wind farms are able to estimate and to optimise the future O&M costs [2]. This methodology together with monitoring of the wind farm should give owners and operators tools to support the decisions in O&M.

In the planning phase of a project a realistic estimate of the expected yearly O&M costs is made which is used together with other costs drivers for the economic assessment. To support the development of the Cost Estimator a realistic offshore wind farm will be considered and used in a case study. For this wind farm an initial O&M cost estimate will be made. This initial cost estimate must be considered as a reference for the case studies supporting the development of the Cost Estimator. Above all the initial cost estimate is used to make a comparison with the actual O&M costs and is the starting point to quantify the effects of modifications in the O&M strategy. For this purpose the calculation model in MS Excel developed by ECN [3, 4] will be used. This model enables to determine the long-term average effort and costs that are needed to maintain the wind farm and to calculate the associated downtime and revenue losses. The process of a maintenance action is depicted in Figure 1.1 and this process has served as the starting point for the development of the ECN model to calculate the initial costs of maintenance.

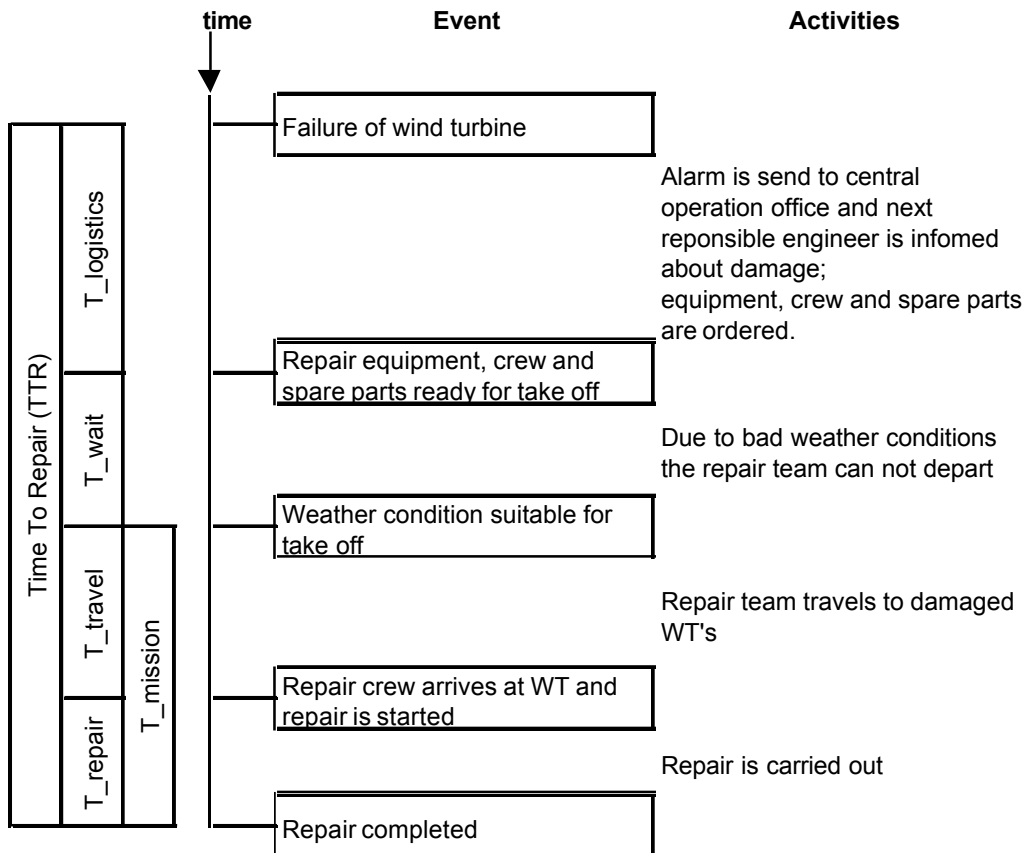


Figure 1.1: Schematic overview of the repair process [3]

As can be seen from Figure 1.1 the Time To Repair (TTR) can be split up into four different time intervals. Especially the waiting time due to bad weather conditions ( $T_{wait}$ ) is of great importance for the total downtime and a lot of research is ongoing in the development of access system with the aim to reduce  $T_{wait}$ . An access system can be characterized by the weather window during which it can be used and the waiting time for a certain device is dependent on the weather window for that device and the duration of the mission ( $T_{mission}$ ).

In the ECN model only the maximal allowable significant wave height and the maximum allowable wind speed are considered, other aspects like fog and ice might be of importance but are not taken into account. To determine the waiting time measured wind and wave data representative for the location of the wind farm have to be considered. To make these wind and wave data applicable for cost modelling the waiting time of a specific system characterised by the maximum allowable wave height and the maximum allowable wind speed has to be specified as a 3rd order polynomial of the mission time. For this purpose first the measured wind and wave measured at a certain location are characterized by means of Weibull distributions, which is described in Chapter 3. Next the waiting time for a specific weather window and the mission time are calculated by means of Monte Carlo simulations based on the previously obtained Weibull distributions, which is described in Chapter 4.

## 1.2 Climate data

For the development of the Cost Estimator climate data are obtained from the wave and wind data published by Rijkswaterstaat for the location “IJmuiden Munitiestortplaats” [5], in the following denoted as YM6, see Figure 1.2. The co-ordinates of YM6 are 52°33’00” east and 4°03’30” north, and the water depth is 21 m.

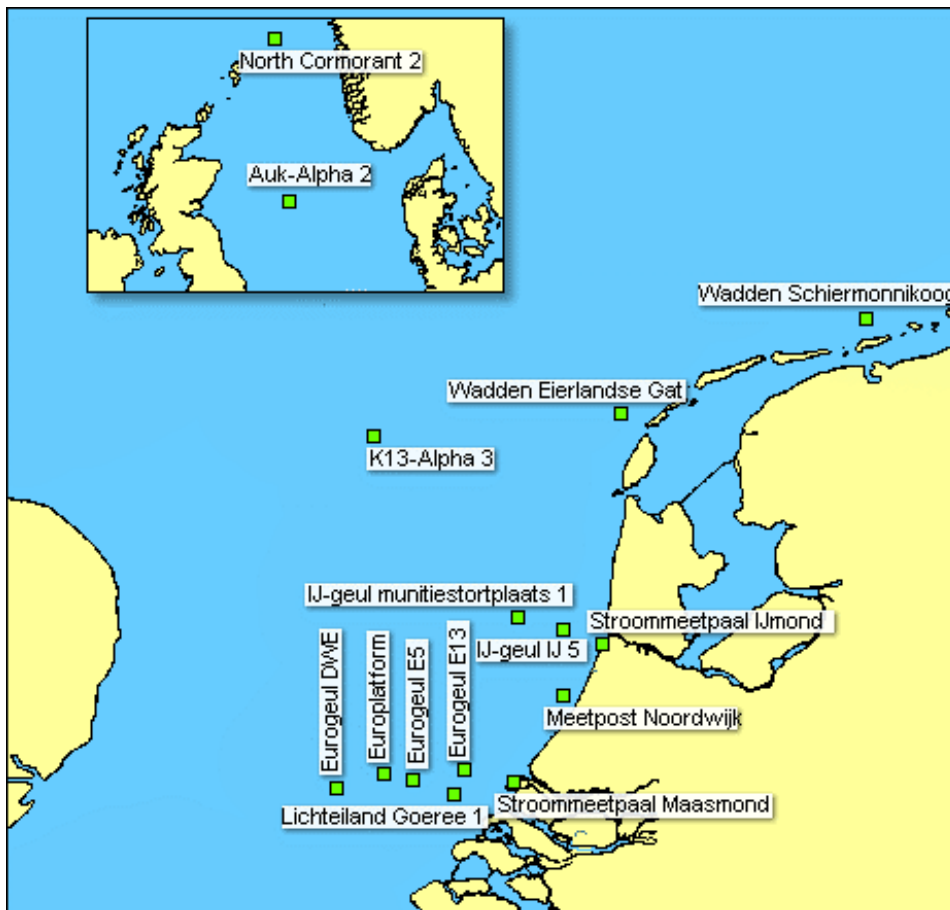


Figure 1.2: Locations for which Rijkswaterstaat measures wind and wave data.



These data are available as 3-hour average values and the wind speed  $V_w$  and the significant wave height  $H_s$  for a period of 12 years (January 1990 - December 2001) have been analysed. The measured data are presented in Chapter 2, where the correlation between the wind and wave data is considered also.

Besides the data over a period of 12 years, the four yearly seasons are considered separately, where these seasons are defined as follows:

- Winter : December, January, February;
- Spring : March, April, May,
- Summer : June, July, August;
- Autumn : September, October, November.

Next these data have been processed to determine the parameters of the Weibull distributions characterising the weather windows specified in Table 1.1, see Chapter 3 and Annex C.

Table 1.1: *Overview of combinations of maximum wind speed and maximum wave height for which the measured time series of YM6 have been processed, the number denotes the weather window number.*

|   |    | Maximum significant wave height, $H_{s,max}$ [m] |   |     |    |    |    |    |    |
|---|----|--|---|-----|----|----|----|----|----|
|   |    | 0.75   | 1 | 1.5 | 2  | 3  | 4  | 5  | 8  |
| Maximum wind speed<br>$V_{w,max}$ [m/s] | 6  | 1  | 4 | 8   | 12 |    |    |    |    |
|   | 8  | 2  | 5 | 9   | 13 | 17 |    |    |    |
|   | 10 | 3  | 6 | 10  | 14 | 18 |    |    |    |
|   | 12 |  | 7 | 11  | 15 | 19 | 22 |    |    |
|   | 15 |  |   |     | 16 | 20 | 23 | 26 |    |
|   | 20 |  |   |     |    | 21 | 24 | 27 | 29 |
|   | 30 |  |   |     |    |    | 25 | 28 | 30 |

Finally the coefficients of the 3rd order polynomials for the waiting time are calculated (see Annex D). An extended evaluation of the waiting times is presented in Chapter 4.



## 2. Evaluation of measured wind and wave data

### 2.1 Wind climate

The 3-hour average wind speed distribution at the location YM6 has been characterized by means of a 2-parameter Weibull distribution. For this purpose the @Risk functionality “Fit Distribution to Data” [6, 7] has been applied to the measured wind data over the period January 1990 up to December 2001. The fit has been made for all data (year) and furthermore the four yearly seasons have been analysed separately. A detailed description of the Weibull distribution is given in Annex A.

The results of the fit procedure are shown in Figure 2.1- Figure 2.5.

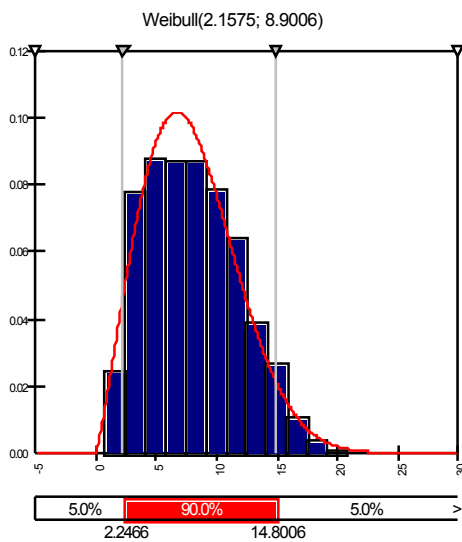


Figure 2.1: *Weibull fit of wind speed distribution in winter*

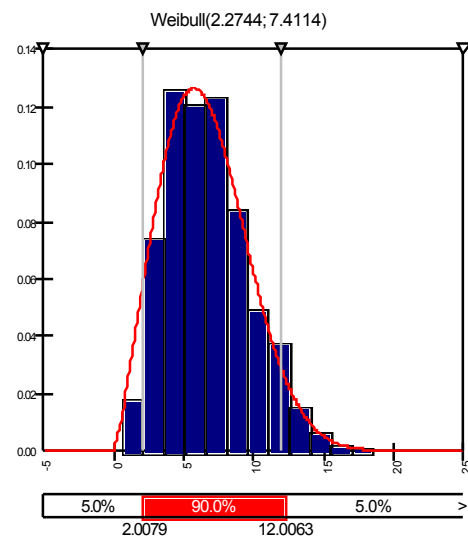


Figure 2.2: *Weibull fit of wind speed distribution in spring*

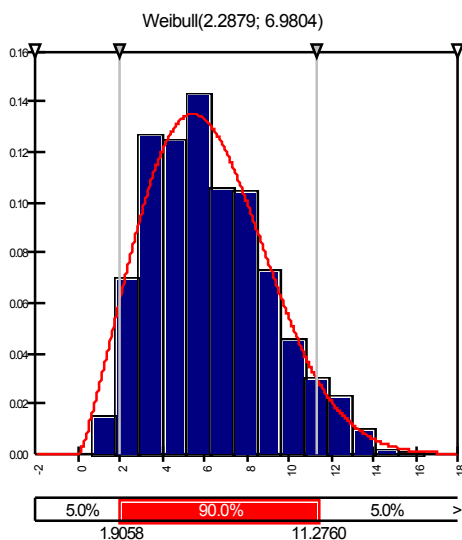


Figure 2.3: *Weibull fit of wind speed distribution in summer*

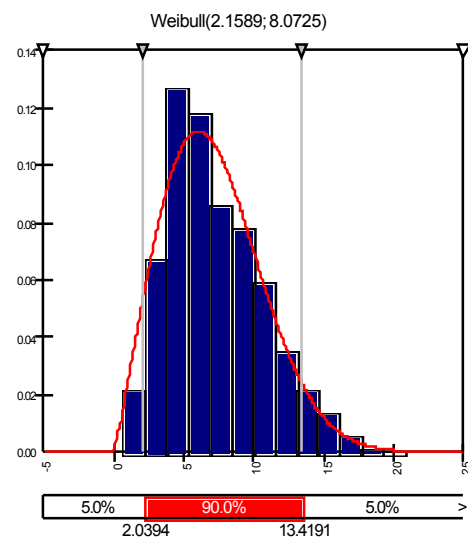


Figure 2.4: *Weibull fit of wind speed distribution in autumn*

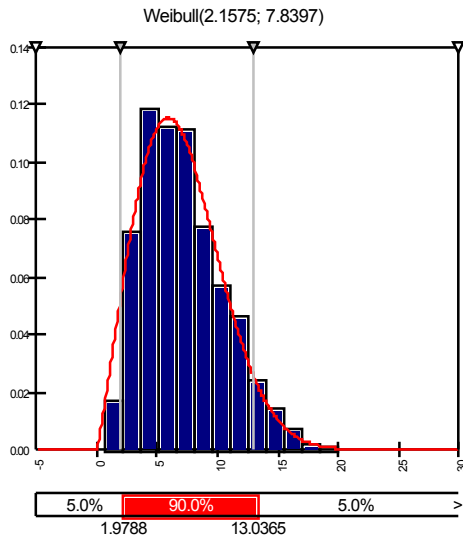


Figure 2.5: *Weibull fit of wind speed distribution over the whole year*

The corresponding cumulative distribution functions are depicted in Figure 2.6 and the calculated Weibull parameters are summarised in Table 2.1. It should be noticed that for an accurate prediction the Weibull parameters should be calculated based on 10-minute mean values. However, only 3-hour data are available for YM6. Although the parameters presented here are less accurate, they are still suitable to determine the capacity factors in the cost model.

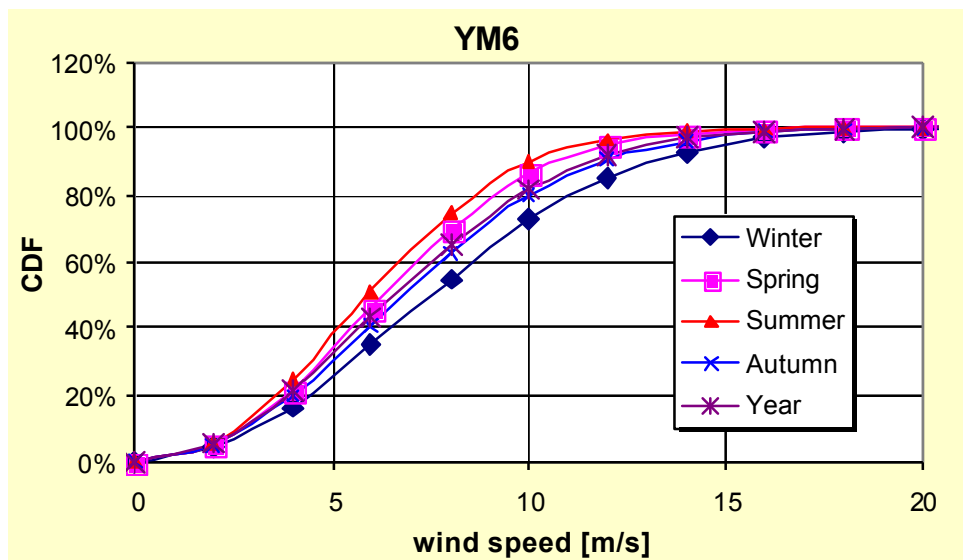


Figure 2.6: *Cumulative distribution functions of the average wind speed distribution at YM6*

Table 2.1: *Weibull parameters of average wind speed distribution at YM6*

|                       | Winter | Spring | Summer | Autumn | Year |
|-----------------------|--------|--------|--------|--------|------|
| shape parameter       | 2.16   | 2.27   | 2.29   | 2.16   | 2.16 |
| scale parameter       | 8.90   | 7.41   | 6.98   | 8.07   | 7.84 |
| mean wind speed [m/s] | 7.88   | 6.57   | 6.18   | 7.15   | 6.94 |

## 2.2 Wave climate

The 3-hour average significant wave height distribution at the location YM6 has been characterised by means of a 2-parameter Weibull distribution too. For this purpose the @Risk functionality “Fit Distribution to Data” [6, 7] has been applied to the measured significant wave height over the period January 1990 up to December 2001. The fit has been made for all data (year) and furthermore the four yearly seasons have been analysed separately. A detailed description of the Weibull distribution is given in Annex A.

The results of the fit procedure are shown in. Figure 2.7 - Figure 2.11

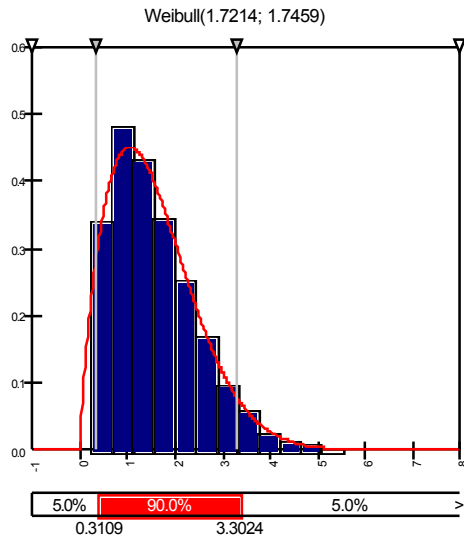


Figure 2.7: *Weibull fit of significant wave height distribution in winter*

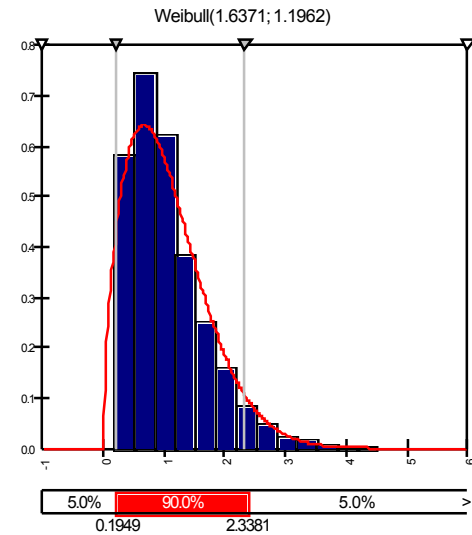


Figure 2.8: *Weibull fit of significant wave height distribution in spring*

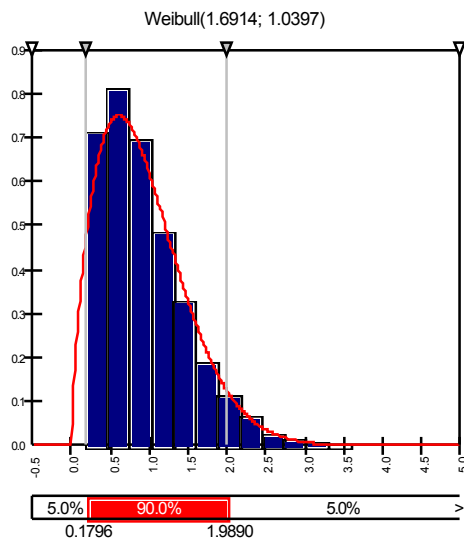


Figure 2.9: *Weibull fit of significant wave height distribution in summer*

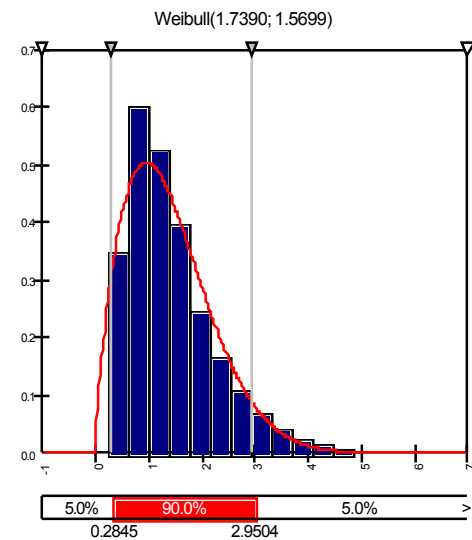


Figure 2.10: *Weibull fit of significant wave height distribution in autumn*

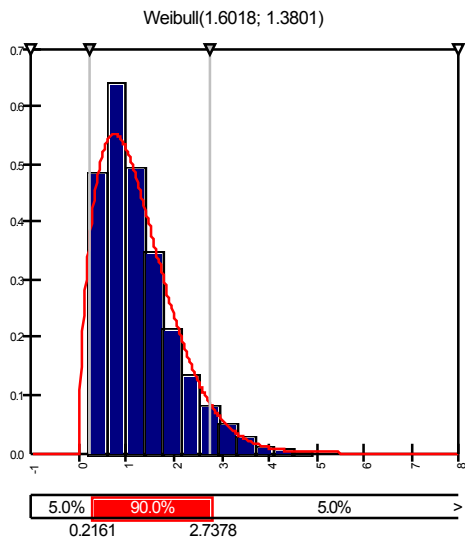


Figure 2.11: *Weibull fit of significant wave height distribution over the whole year*

The corresponding cumulative distribution functions are depicted in Figure 2.12 and the calculated Weibull parameters are summarised in Table 2.2

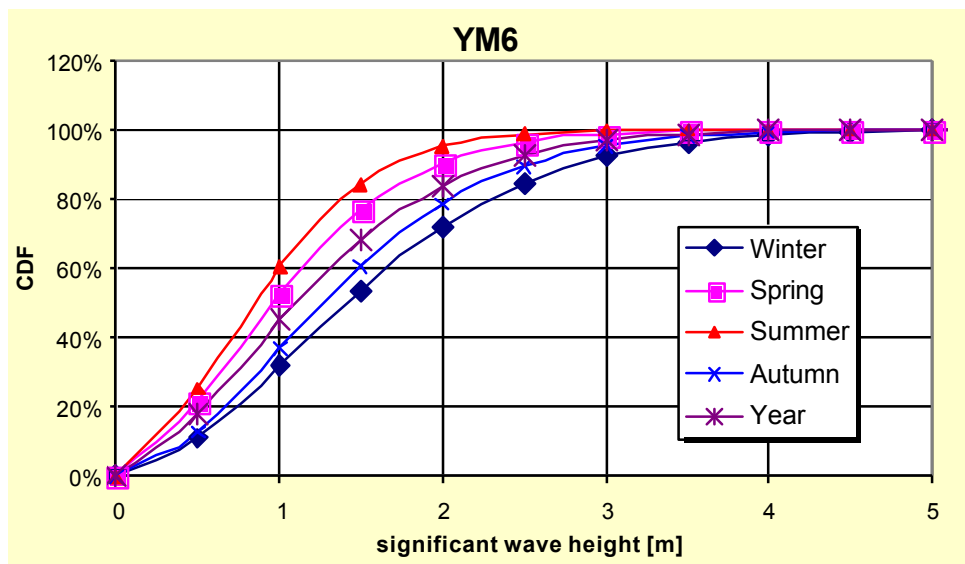


Figure 2.12: *Cumulative distribution functions of the significant wave height distribution at YM6*

Table 2.2: *Weibull parameters of the significant wave height distribution at YM6*

|                      | Winter | Spring | Summer | Autumn | Year |
|----------------------|--------|--------|--------|--------|------|
| shape                | 1.72   | 1.64   | 1.69   | 1.74   | 1.60 |
| scale                | 1.75   | 1.20   | 1.04   | 1.57   | 1.38 |
| mean wave height [m] | 1.56   | 1.07   | 0.93   | 1.40   | 1.24 |

### 2.3 Combined wind and wave data

The correlation between the 3-hour average wind speed and the 3-hour average significant wave height over the period Jan. 1990 - Dec. 2001 is shown in Figure 2.13. Similar plots are obtained when the four yearly seasons are considered separately. It is clear that the wave height and the wind speed are strongly correlated. In Figure 2.13 two regions can be distinguished; the upper region where the wind speed is relative low and the wave height is relative high and the lower region where the wind speed is relative high and the wave height is relative low. In the upper region the wind speed will be the determinative parameter, while in the lower region it is the wave height. This can be explained as follows. For instance consider a wind speed of 10 m/s. It appears that for wind speeds up to 10 m/s the wave height will be less than 2.5 m with a very high probability. So variations of wave height in the interval greater than approximately 2.5 m will not influence the length of the weather windows. For the lower region it holds that very high wind speeds do not occur simultaneously with low wave heights, hence the wave height is the determinative parameter in this region.

In Annex B the frequency of occurrence of combinations of wind speed and significant wave height are given for the four yearly seasons and the whole year.

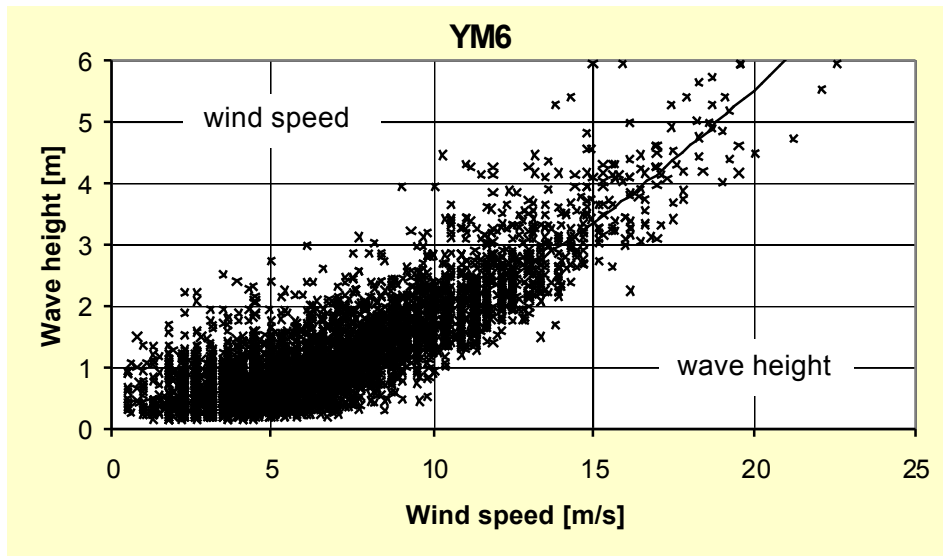


Figure 2.13: Measured significant wave height as function of the measured wind speed for the period Jan. 1990 - Dec. 2001





### 3. Weather Windows

#### 3.1 General description

The maximum significant wave height  $H_{s,max}$  and the maximum wind speed  $V_{w,max}$  during which a certain maintenance action can be performed are of large influence on the downtime after a failure. If a failure occurs, the repair action can only be initiated if the weather conditions are suitable. If not, the repair has to be postponed. It is not only sufficient that the right weather window occurs, the duration should also be long enough to make sure that the repair can be carried out.

To illustrate this, a small part of a time series for the wind speed  $V_w$  and the significant wave height  $H_s$  are plotted in Figure 3.1. As an example it is assumed that a repair action can be carried out only if both  $H_s \leq 1.5$  m and  $V_w \leq 12$  m/s, hence the lines corresponding with  $V_{w,max} = 12$  m/s and  $H_{s,max} = 1.5$  m are drawn too. At the horizontal axis corresponding with the minimum  $y$ -value ( $V = 0$  m/s) the low time intervals are indicated. During a low time interval  $V_w \leq V_{w,max}$  and  $H_s \leq H_{s,max}$  and repair is possible provided that the length of the interval is sufficient to complete the mission. At the horizontal axis corresponding with the maximum  $y$ -value ( $V = 25.0$  m/s) the high time intervals are indicated. During a high time interval  $V_w > V_{w,max}$  or  $H_s > H_{s,max}$  and it is not allowed for the chosen device to leave the port or to be in operation. From Figure 3.1 it can be seen that if the failure occurs at  $t = 0$ , it takes approximately 96 hours before a repair action of 40 hours can be carried out. If the duration of the repair is only 20 hours, the waiting time is approximately 56 hours. Since the failure can occur at any point in time, the waiting time until a suitable weather window occurs in fact is a stochastic variable.

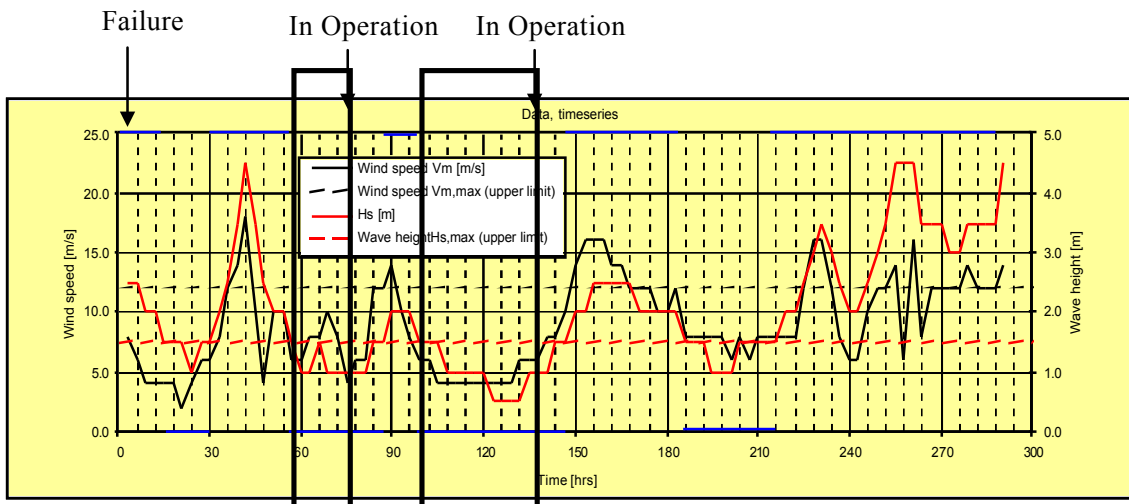


Figure 3.1: Example of determination of waiting time for a maintenance action that can be carried out if  $H_s \leq 1.5$  m and  $V_w \leq 12$  m/s and the duration is 20 hrs or 40 hrs

#### 3.2 Characterisation of weather windows

Due to the stochastic behaviour of the waiting time it is not practical in the cost modelling to work with measured time series because of the amount of data to be handled repeatedly. To characterize long term wind and wave characteristics, data representative for the location of the wind farm should be analysed to search for the following variables:

- number of times that suitable weather windows occur, i.e.  $H_s$  and  $V_w$  are below the maximum values;
- duration of these suitable weather windows;
- number of times that weather windows occur during which maintenance cannot be carried out;
- duration of these weather windows that in fact determine the waiting time.

The length of the  $i^{\text{th}}$  low interval is indicated by  $T_i^{\text{low}}$  and covers the time interval starting on  $t_{i,1}^{\text{low}}$  and ending on  $t_{i,2}^{\text{low}}$ . The same definition holds for the high intervals.

The probability that a failure does occur in a low interval or a high interval is now given by

$$P_{\text{low}} = 1 - P_{\text{high}} = \frac{\sum T_i^{\text{low}}}{\sum T_i^{\text{low}} + \sum T_i^{\text{high}}}$$

To determine the first low interval in which a repair may be carried out it is not only of importance whether the interval in which the failure did occur is low or high, but the length of this interval is of importance also just as the length of the subsequent intervals. So the length of the 1st interval has been determined. As failures occur randomly one is interested in the probability that the point of time at which the failure occurs lies in an interval with a certain length. The probability that a failure occurs in a low interval with a certain length is determined by the fraction of the total duration of all low intervals with this length compared to total duration of all low intervals considered. For instance  $n_k^{\text{low}}$  low intervals with a length of  $T_k^{\text{low}}$  are found. In case the 1st interval is low the probability that this interval has length  $T_k^{\text{low}}$  is now

$$\frac{n_k^{\text{low}} \cdot T_k^{\text{low}}}{\sum T_i^{\text{low}}}$$

The same holds for the high intervals. In this way the statistical distribution function of the length of the intervals can be determined for the low intervals as well as for the high intervals. The corresponding cumulative distribution function (CDF) is denoted by  $F_D^{\text{low}}(T)$  for the low intervals and by  $F_D^{\text{high}}(T)$  for the high intervals and gives the probability that a certain point in time lies in an interval with a length less than  $T$ .

The subsequent intervals do occur randomly, so the length is determined by the fraction of the number of intervals with a certain length compared to the total number of low or high intervals. The probability that the length of next low interval equals  $T_k^{\text{low}}$  is now given by

$$\frac{n_k^{\text{low}}}{\sum n_i^{\text{low}}}$$

The same holds for the high intervals. In this way the statistical distribution function of the number of the intervals can be determined for the low intervals as well as for the high intervals. This cumulative distribution function (CDF) is denoted by  $F_N^{\text{low}}(T)$  for the low intervals and by  $F_N^{\text{high}}(T)$  for the high intervals and gives the probability that the length of a randomly chosen interval is less than  $T$ .

So, to determine  $P_{\text{low}}$  or  $P_{\text{high}}$  and the cumulative distribution functions  $F_D^{\text{low}}(T)$ ,  $F_D^{\text{high}}(T)$ ,  $F_N^{\text{low}}(T)$  and  $F_N^{\text{high}}(T)$  the quantities  $n_k^{\text{low}}$ ,  $n_k^{\text{high}}$ ,  $T_k^{\text{low}}$  and  $T_k^{\text{high}}$  have to be calculated from the time series of the wind speed and the wave height.

For this purpose the times series of the wind speed and the wave height have to be processed to determine the low and the high intervals and subsequently corresponding cumulative distribution function.

For this purpose the computer program WeWiCDF has been developed at ECN [3]. In this program, which is implemented in an Excel workbook, time series of measured wind and wave data are processed to determine the low and the high intervals given the limit values  $V_{w,max}$  and  $H_{s,max}$ . Furthermore these low and high intervals are processed by means of pivot tables to calculate the number of occurrences, finally resulting in tabulated cumulative distribution functions for  $F_D^{low}(T)$ ,  $F_D^{high}(T)$ ,  $F_N^{low}(T)$  and  $F_N^{high}(T)$ .

The tabulated CDF's are fitted by a Weibull distribution by means of the @Risk function "Fit distribution to data" and the shape parameter and the scale parameter are obtained. Although several statistical functions showed a good agreement it appeared that the Weibull distribution could be used for all data sets (duration and length of intervals for both high and low) [8].

The parameters  $P_{low}$  and the parameters for the cumulative distribution functions  $F_D^{low}(T)$ ,  $F_D^{high}(T)$ ,  $F_N^{low}(T)$  and  $F_N^{high}(T)$  are calculated taking into account the wind speed and wave height data for all yearly seasons, resulting in yearly parameters. Furthermore the data of four yearly seasons are treated separately resulting in four sets of parameters valid for a certain season.

### 3.3 Data

The 3 hour mean wind speed and the 3 hour significant wave height published for YM 6 for the period 1991 - 2001 have been processed in the way described above for the combinations of maximum wind speed and maximum wave height listed in Table 1.1.

The calculated Weibull parameters for the weather windows specified in Table 1.1 are given in Annex B.



## 4. Waiting Time

### 4.1 Model description

To determine the duration of the waiting phase ( $T_{\text{wait}}$ ) for a certain mission with length  $T_{\text{mission}}$  (see Figure 1.1) the Excel workbook  $T_{\text{wait}}$  has been developed at ECN [3]. In this workbook a stylistic time series consisting of alternately low and high intervals is constructed. For this purpose an @Risk model has been developed [3] based on  $P_{\text{low}}$  and on the Weibull distributions of  $F_D^{\text{low}}(T)$ ,  $F_D^{\text{high}}(T)$ ,  $F_N^{\text{low}}(T)$ , and  $F_N^{\text{high}}(T)$ , which are described in Chapter 3. The shape and the scale parameters for these Weibull distributions are summarized in Annex C. The construction is done according to the scheme shown in Figure 4.1. To determine whether the first interval is low or high the RiskBinomial function is applied, while the length of the intervals is determined by the @Risk function RiskWeibull together with the appropriate parameters.

The first low interval  $T_i^{\text{low}}$  with a length greater than  $T_{\text{mission}}$  is looked up and the waiting time now equals  $t_{i,1}^{\text{low}}$ .

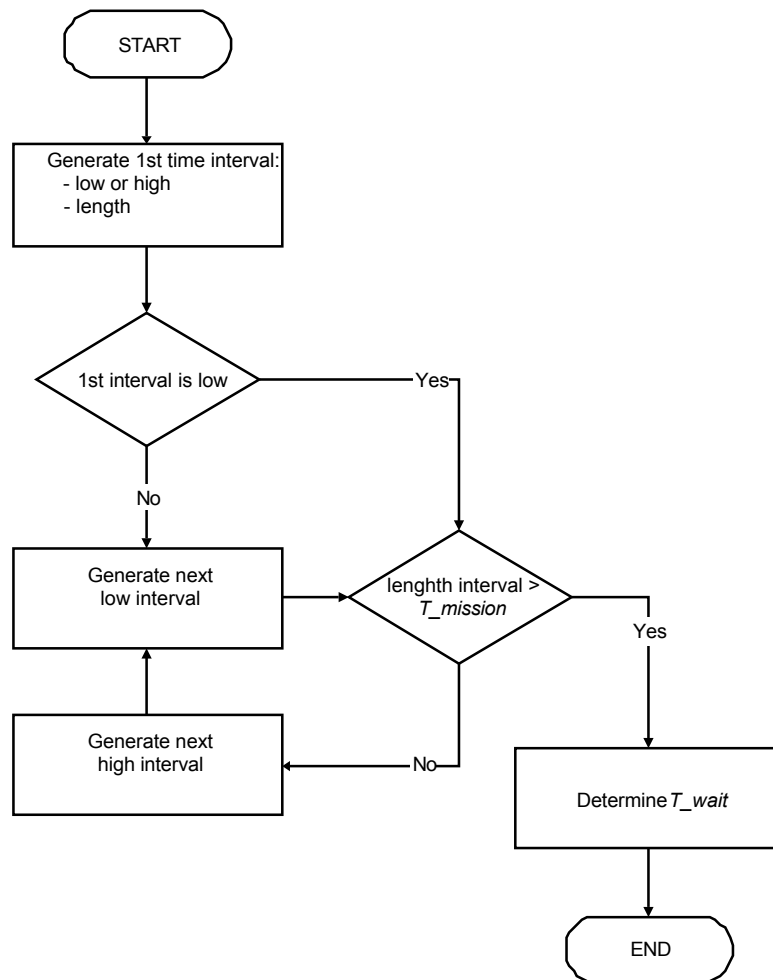


Figure 4.1: Procedure for generating stylistic time series of alternately low and high intervals.

As the input for this model is based on stochastic variables the result  $T_{wait}$  will be a stochastic quantity also, and the statistical parameters, like the mean value and the standard deviation of  $T_{wait}$  are of interest. The mean value and the standard deviation of  $T_{wait}$  for a certain value of  $T_{mission}$  are determined by means of Monte Carlo simulation available in @Risk, where the  $T_{Wait}$  is determined by the @Risk function RiskOutput.

After performing analyses for several values of  $T_{mission}$  the resulting mean values and standard deviation can be given as function of  $T_{mission}$ . The mean values and the standard deviation calculated for a certain weather window can now be fitted by a 2nd or 3rd order polynomial, so that the mean value and the standard deviation for a certain weather window are available as a continuous function of the duration of the mission. It is clear that the waiting time will increase when the duration of the mission increases, hence the polynomial fits should be continuously increasing function of the mission time. As an example the waiting time as function of the duration of the mission is shown in Figure 4.2 for a device that is able to operate for wind speeds up to 8 m/s and wave heights up to 1.5 m, where the wind and wave data over the whole year have been considered. Since the waiting time is a stochastic value, the standard deviation, the 5% value and the 95% value are given also. Furthermore the polynomial fitted through the calculated mean values and the calculated standard deviations are shown.

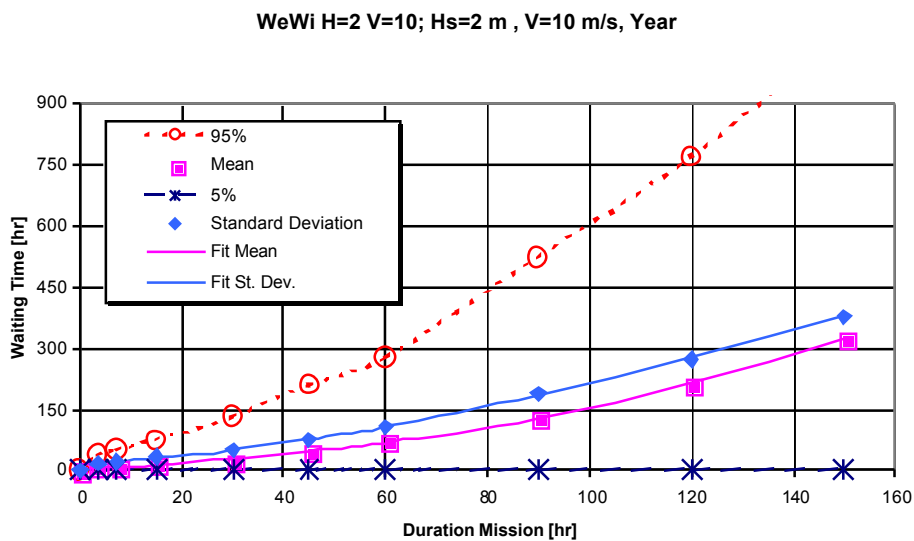


Figure 4.2: *Waiting time as function of the duration of the mission*

## 4.2 Results

For the combinations of  $H_s$  and  $V_w$  summarised in Table 1.1 the mean value of the waiting time has been calculated as function of the duration of the mission similar to Figure 4.2 and the results have been fitted by a polynomial. The coefficient of these polynomials are summarised in Annex D for the four yearly seasons and for the whole year.

To show the characteristics of the waiting time it has been plotted as function of wave height for several different wind speeds in Figure 4.3 and as function of the wind speed for different values of the wave height in Figure 4.4. In both figures the duration of the mission is assumed to be 10 hours. These figure are based on the wind and wave data of the whole year for the period Jan. 1990 - Dec. 2001. The same results are presented in Figure 4.5 where the waiting time is given in a 3D plot as function of both the wind speed and the wave height. Besides a mission with duration of 10 hours missions with a duration of 25, 50 and 100 hours are depicted also. Similar results are obtained when the data for a specific yearly season is considered. In Figure 4.6 the influence of the seasons is shown

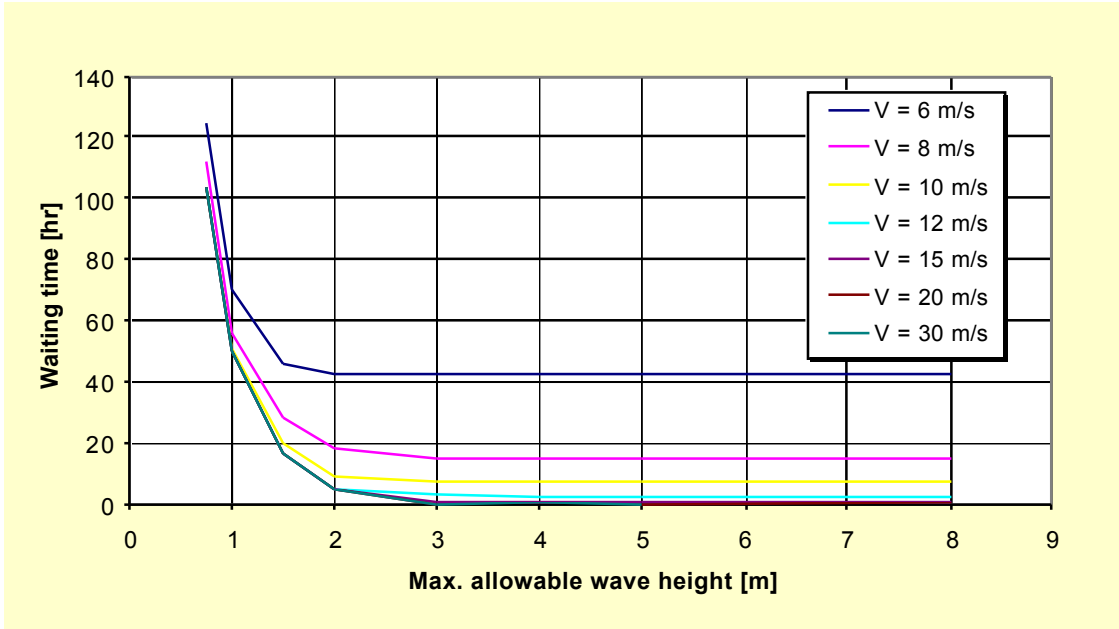


Figure 4.3: *Waiting time as function of the maximum allowable wave height for several values of the maximum allowable wind speed; duration of the mission is 10 hours, wind and wave data of the whole year*

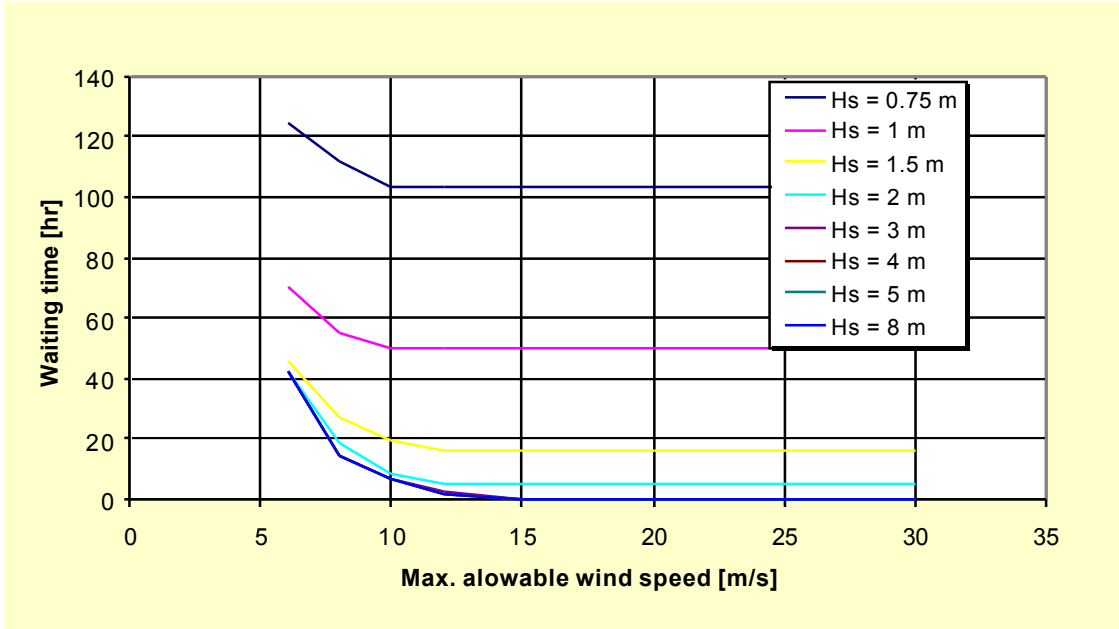


Figure 4.4: *Waiting time as function of the maximum allowable wind speed for several values of the maximum allowable wave height; duration of the mission is 10 hour, wind and wave data of the whole year*

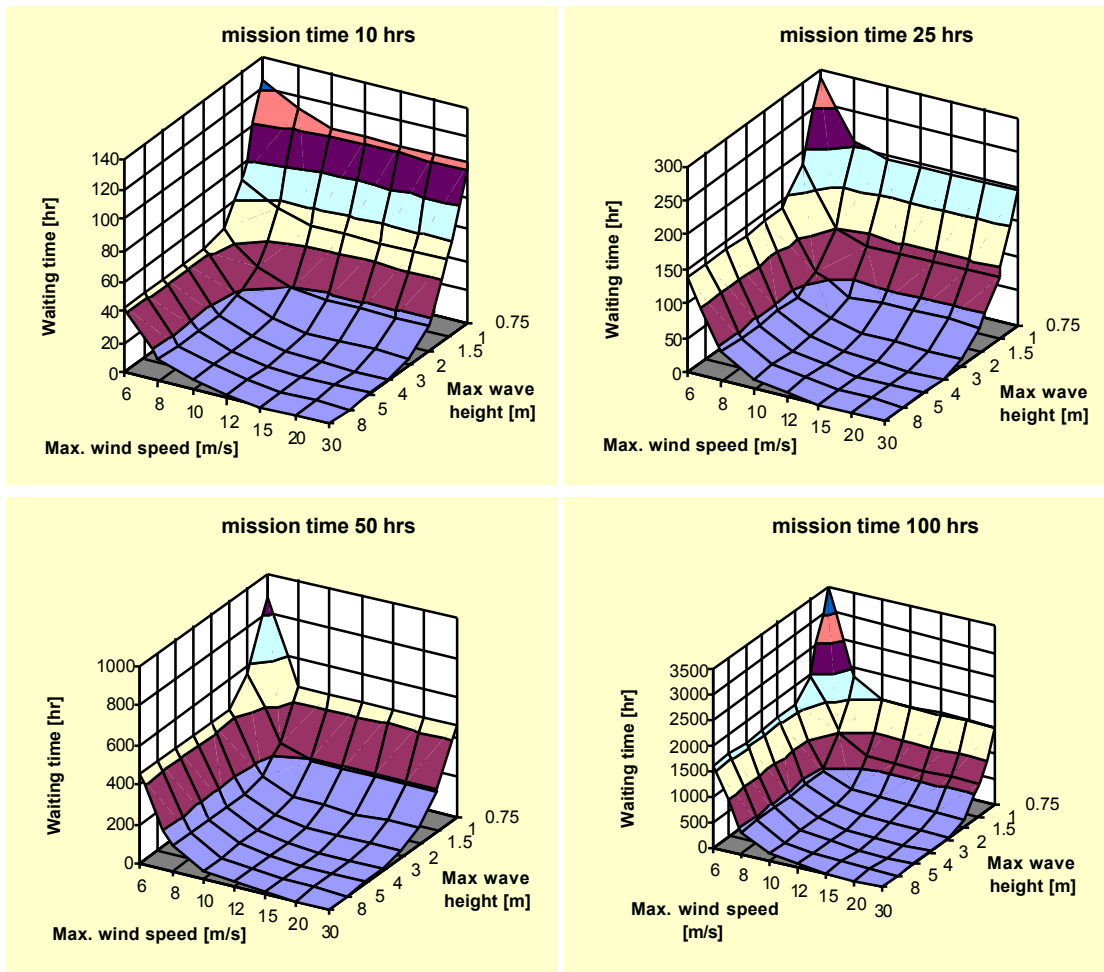


Figure 4.5: *Waiting time as function of the maximum allowable wave height and the maximum allowable wind speed for several values of the duration of the mission; wind and wave data of the whole year*

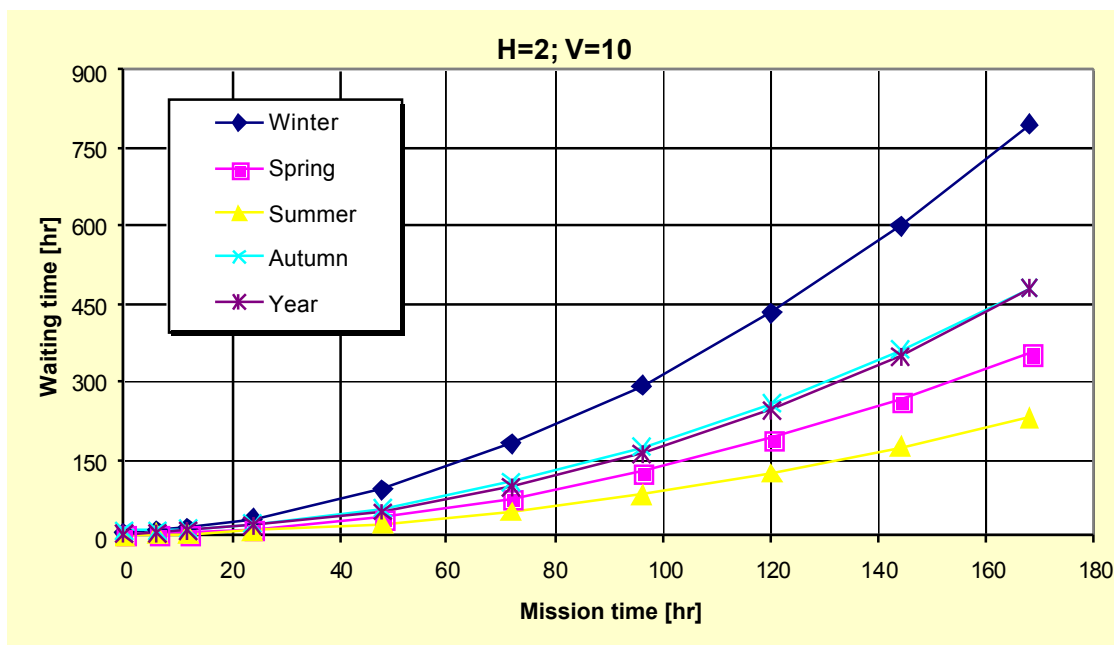


Figure 4.6: *Influence of the season on the waiting time; ( $H_s = 2$  m;  $V_w = 10$  m/s)*



As expected the waiting time decreases when the weather windows become less harsh. This decrease is most significant for wave heights up to 1,5 - 2 m and wind speeds up to 10 - 12 m/s. So using access systems that can operate up to wave heights of 2 m and wind speeds up to 12 m/s will have a strong positive effect on the waiting time. Investment in access system that can operate at wave heights above 2 m and at wind speeds above 12 m/s should be considered very careful for this location. In general the advantage in terms of waiting time is only limited. However depending on the number of times and the duration a device is needed it might be advantageous in specific situations.



## 5. Conclusions

After a failure, an offshore wind turbine may be out of operation for a significant period because it can not be accessed due to bad weather conditions. To be able to estimate this downtime the offshore weather conditions at the location of the wind farm have to be analysed. In this report the 3-hour average wind and wave data measured by Rijkswaterstaat for the location Munitiestortplaats IJmuiden (YM6) over the period January 1990 - December 2001 have been analysed.

To calculate the revenue losses due to downtime the capacity factor of the wind turbine has to be determined. For this purpose the wind speed distribution at YM6 is described by a 2-parameter Weibull distribution. Generally this Weibull distribution is based on 10-minute average wind speed data. However, 3-hour average data are available only so that the Weibull parameters of the wind speed distribution are based on these 3-hour average data. Besides the data over a period of 12 years also the four yearly seasons are considered separately.

The capabilities of an access system are particularly dependent on the weather window in which it can be operated. The weather window of an access system is characterized by the maximum significant wave height  $H_{s,max}$  and the maximum wind speed  $V_{w,max}$  during which a certain maintenance action can be performed. For a number of different weather windows the waiting time due to bad weather conditions has been calculated and logically the waiting time decreases when the weather windows become less harsh. It appears that this decrease is most significant for wave heights up to 1,5 - 2 m and wind speeds up to 10 - 12 m/s. So using access systems that can operate up to wave heights of 2 m and wind speeds up to 12 m/s will have a strong positive effect on the down time for this location. On the other hand it is questionable whether an investment in access system that can operate at wave heights above 2 m and at wind speeds above 12 m/s should be made for this location. In general the advantage in terms of waiting time is only limited. However depending on the number of times and the duration a device is needed it might be advantageous in specific situations.

## References

- [1] L.W.M.M. Rademakers, H. Braam, T.W. Verbruggen, “*R&D Needs for O&M of Wind Turbines*”, ECN-RX--03-045
- [2] Project proposal Development of O&M Cost Estimator for Offshore Wind Farms, [www.ecn.nl/extranet/omce](http://www.ecn.nl/extranet/omce)
- [3] H. Braam, L. Rademakers, “*Models to analyse operation and maintenance aspects of offshore wind farms, User Guide and model Description*”, ECN-CX--04-047, June 2004
- [4] L.W.M.M. Rademakers, H. Braam, M.B. Zaaijer, G.J.W. van Bussel, “*Assessment and Optimisation of Operation and Maintenance of Offshore Wind Turbines*”, Proc. EWEC 2003, Madrid.
- [5] Ministerie van Verkeer en Waterstaat, Monitoring van de Waterstaatkundige Toestand des Lands (MWTL), data YM6, [www.golflimaat.nl](http://www.golflimaat.nl)
- [6] “*Guide to using @Risk, version 4*”, Palisade Corporation, April 2004
- [7] D. Vose, “*Risk Analysis; A Quantitative Guide*”, 2nd ed., 2000, John Wiley & Sons Ltd; ISBN 0-471-99765-X
- [8] L. Rademakers, et al, “*Lightning damage of OWECS, Part 1: Parameters Relevant for Cost Modelling*”, ECN-C--02-053, June 2002

## Annex A: Weibull distribution

The cumulative distribution function (CDF) of the Weibull distribution is defined as

$$F_X(x) = 1 - e^{-\left(\frac{x}{b}\right)^a}, x > 0 \quad (\text{A.1})$$

where:

$\alpha$  : shape parameter ( $\alpha > 0$ );

$\beta$  : scale parameter ( $\beta > 0$ ).

The mean value reads

$$m = \frac{b}{a} \Gamma\left(\frac{1}{a}\right) \quad (\text{A.2})$$

and the standard deviation reads

$$s = \sqrt{\frac{b^2}{a} \left[ 2\Gamma\left(\frac{2}{a}\right) - \frac{1}{a} \Gamma^2\left(\frac{1}{a}\right) \right]} \quad (\text{A.3})$$

where  $\Gamma$  is the gamma function defined by

$$\Gamma(x) = \int_0^{\infty} e^{-t} t^{x-1} dt \quad (\text{A.4})$$

Integration by parts gives the important functional relation of the gamma function

$$\Gamma(x+1) = x\Gamma(x) \quad (\text{A.5})$$

Given the mean value and the standard deviation the Weibull parameters can be calculated as follows. From Eq. (A.2) and (A.3) it can be deduced that

$$\left(\frac{s}{m}\right)^2 = \frac{\frac{2}{a} \Gamma\left(\frac{2}{a}\right)}{\left(\frac{1}{a}\right)^2 \Gamma^2\left(\frac{1}{a}\right)} \quad (\text{A.6})$$

which gives the value for the shape parameter. Next the scale parameter is calculated with Eq. (A.2)

$$b = \frac{m}{\frac{1}{a} \Gamma\left(\frac{1}{a}\right)} \quad (\text{A.7})$$



## Annex B: Correlation of wind speed and wave height

For the location YM6 the frequency of occurrence of combinations of wind speed and significant wave height over the period Jan. 1990 - Dec. 2001 are given below. Please note that these tables should not be mixed up with scatter plots in which the occurrence frequency of the significant wave height and the zero crossing period are plotted. In these type of scatter plots the wind speed is not considered.

| Winter                            |    | significant wave height, Hs [m] - upper limi |      |      |      |      |     |     |     |     |    |     |    |     | Grand Total |      |      |
|-----------------------------------|----|--|------|------|------|------|-----|-----|-----|-----|----|-----|----|-----|-------------|------|------|
|                                   |    | 0.5  | 1    | 1.5  | 2    | 2.5  | 3   | 3.5 | 4   | 4.5 | 5  | 5.5 | 6  | 6.5 |             | 7    |      |
| wind speed, Vw [m/s] - upperlimit | 2  | 111  | 117  | 28   | 6    | 3    | 1   |     |     |     |    |     |    |     |             |      | 266  |
|                                   | 4  | 498  | 580  | 177  | 35   | 9    | 3   |     |     |     |    |     |    |     |             |      | 1302 |
|                                   | 6  | 214  | 751  | 431  | 105  | 19   | 3   |     |     |     |    |     |    |     |             |      | 1523 |
|                                   | 8  | 17   | 544  | 649  | 295  | 74   | 19  | 7   |     |     |    |     |    |     |             |      | 1605 |
|                                   | 10 |  | 91   | 454  | 507  | 208  | 56  | 19  | 4   | 2   |    | 1   |    |     |             |      | 1342 |
|                                   | 12 |  | 5    | 150  | 418  | 392  | 153 | 53  | 18  | 8   |    | 3   |    |     |             |      | 1200 |
|                                   | 14 |  | 1    | 5    | 113  | 267  | 245 | 111 | 45  | 15  | 4  | 3   |    |     | 1           |      | 810  |
|                                   | 16 |  |      |      | 5    | 53   | 114 | 121 | 55  | 32  | 19 | 10  | 3  | 1   |             |      | 413  |
|                                   | 18 |  |      |      |      | 1    | 18  | 55  | 25  | 19  | 10 | 7   | 4  | 3   | 1           |      | 143  |
|                                   | 20 |  |      |      |      |      |     | 5   | 7   | 12  | 12 | 4   | 5  | 1   |             |      | 46   |
|                                   | 22 |  |      |      |      |      |     |     |     | 2   | 2  | 6   |    |     |             |      | 10   |
|                                   | 24 |  |      |      |      |      |     |     |     |     |    |     | 1  | 2   |             |      | 3    |
|                                   | 26 |  |      |      |      |      |     |     |     |     |    |     |    |     | 1           |      | 1    |
| Grand Total                       |    | 840  | 2089 | 1894 | 1484 | 1026 | 612 | 371 | 156 | 90  | 51 | 29  | 14 | 7   | 1           | 8664 |      |

| Spring                            |    | significant wave height, Hs [m] - upper limi |      |      |     |     |     |     |    |     |   |     |   |     | Grand Total |      |      |
|-----------------------------------|----|--|------|------|-----|-----|-----|-----|----|-----|---|-----|---|-----|-------------|------|------|
|                                   |    | 0.5  | 1    | 1.5  | 2   | 2.5 | 3   | 3.5 | 4  | 4.5 | 5 | 5.5 | 6 | 6.5 |             | 7    |      |
| wind speed, Vw [m/s] - upperlimit | 2  | 191  | 128  | 21   | 7   |     |     |     |    |     |   |     |   |     |             |      | 347  |
|                                   | 4  | 715  | 633  | 159  | 19  | 3   | 2   | 1   |    |     |   |     |   |     |             |      | 1532 |
|                                   | 6  | 667  | 1111 | 416  | 75  | 7   | 3   |     |    |     |   |     |   |     |             |      | 2279 |
|                                   | 8  | 200  | 985  | 659  | 191 | 32  | 5   | 2   |    |     |   |     |   |     |             |      | 2074 |
|                                   | 10 | 25   | 315  | 517  | 350 | 95  | 21  | 4   |    |     |   |     |   |     |             |      | 1327 |
|                                   | 12 |  | 33   | 177  | 289 | 189 | 69  | 24  | 7  | 5   |   |     |   |     |             |      | 793  |
|                                   | 14 |  | 1    | 14   | 62  | 116 | 64  | 43  | 12 | 7   | 2 |     |   |     |             |      | 321  |
|                                   | 16 |  |      |      | 2   | 26  | 38  | 22  | 12 | 8   | 2 |     |   |     |             |      | 110  |
|                                   | 18 |  |      |      |     |     | 6   | 7   | 10 | 8   |   | 1   |   |     |             |      | 32   |
|                                   | 20 |  |      |      |     |     | 1   | 3   | 4  | 3   |   |     |   |     |             |      | 11   |
|                                   | 22 |  |      |      |     |     |     |     |    |     | 2 | 2   |   |     |             |      | 4    |
|                                   | 24 |  |      |      |     |     |     | 1   |    |     |   |     |   |     |             |      |      |
|                                   | 26 |  |      |      |     |     |     |     |    |     |   |     |   |     |             |      |      |
| Grand Total                       |    | 1798   | 3206 | 1963 | 995 | 468 | 210 | 106 | 45 | 31  | 6 | 3   |   |     |             | 8831 |      |

| Autumn                            |    | significant wave height, Hs [m] - upper limi |      |      |      |     |     |     |     |     |    |     |   |     | Grand Total |      |      |
|-----------------------------------|----|--|------|------|------|-----|-----|-----|-----|-----|----|-----|---|-----|-------------|------|------|
|                                   |    | 0.5  | 1    | 1.5  | 2    | 2.5 | 3   | 3.5 | 4   | 4.5 | 5  | 5.5 | 6 | 6.5 |             | 7    |      |
| wind speed, Vw [m/s] - upperlimit | 2  | 102  | 107  | 38   | 10   | 2   |     |     |     |     |    |     |   |     |             |      | 259  |
|                                   | 4  | 431  | 754  | 188  | 51   | 17  | 3   | 1   | 3   |     |    |     |   |     |             |      | 1448 |
|                                   | 6  | 291  | 1109 | 515  | 111  | 28  | 5   | 3   | 4   | 1   |    |     |   |     |             |      | 2067 |
|                                   | 8  | 38   | 548  | 827  | 317  | 63  | 17  | 3   | 2   |     |    |     |   |     |             |      | 1815 |
|                                   | 10 | 1  | 76   | 488  | 489  | 156 | 54  | 11  | 4   | 1   |    |     |   |     |             |      | 1280 |
|                                   | 12 |  | 7    | 86   | 350  | 313 | 113 | 47  | 12  | 4   |    |     |   |     |             |      | 932  |
|                                   | 14 |  |      | 6    | 37   | 180 | 203 | 71  | 35  | 15  | 5  | 1   |   |     |             |      | 553  |
|                                   | 16 |  |      |      | 7    | 14  | 58  | 90  | 46  | 24  | 11 |     | 1 |     |             |      | 251  |
|                                   | 18 |  |      |      |      | 1   | 7   | 28  | 31  | 19  | 8  | 1   | 1 |     |             |      | 96   |
|                                   | 20 |  |      |      |      |     |     | 3   | 8   | 9   | 7  |     | 2 |     |             |      | 29   |
|                                   | 22 |  |      |      |      |     |     |     | 1   | 1   | 2  |     |   |     |             |      | 4    |
|                                   | 24 |  |      |      |      |     |     |     |     | 1   |    |     |   |     |             |      | 1    |
|                                   | 26 |  |      |      |      |     |     |     |     |     |    |     |   |     |             |      |      |
| Grand Total                       |    | 863  | 2601 | 2148 | 1372 | 774 | 460 | 257 | 146 | 75  | 33 | 2   | 4 |     |             | 8735 |      |

| Year                               |    | significant wave height, Hs [m] - upper lim |       |      |      |      |      |     |     |     |    |     |    |     | Grand Total |       |      |
|------------------------------------|----|---|-------|------|------|------|------|-----|-----|-----|----|-----|----|-----|-------------|-------|------|
|                                    |    | 0.5   | 1     | 1.5  | 2    | 2.5  | 3    | 3.5 | 4   | 4.5 | 5  | 5.5 | 6  | 6.5 |             | 7     |      |
| wind speed, Vw [m/s] - upper limit | 2  | 676   | 472   | 109  | 24   | 5    | 1    |     |     |     |    |     |    |     |             |       | 1287 |
|                                    | 4  | 2624  | 2663  | 648  | 112  | 29   | 8    | 3   | 3   |     |    |     |    |     |             |       | 6090 |
|                                    | 6  | 2039  | 4070  | 1733 | 325  | 57   | 13   | 3   | 4   | 1   |    |     |    |     |             |       | 8245 |
|                                    | 8  | 475   | 3044  | 2730 | 950  | 179  | 43   | 14  | 2   |     |    |     |    |     |             |       | 7437 |
|                                    | 10 | 56  | 798   | 2039 | 1647 | 512  | 134  | 36  | 8   | 3   |    | 1   |    |     |             |       | 5234 |
|                                    | 12 |   | 71    | 624  | 1339 | 1019 | 359  | 127 | 38  | 17  |    | 3   |    |     |             |       | 3597 |
|                                    | 14 |   | 2     | 31   | 261  | 689  | 560  | 253 | 100 | 37  | 11 | 4   |    | 1   |             |       | 1949 |
|                                    | 16 |   |       |      | 15   | 101  | 237  | 247 | 115 | 65  | 32 | 10  | 4  | 1   |             |       | 827  |
|                                    | 18 |   |       |      |      | 3    | 36   | 94  | 69  | 46  | 18 | 9   | 5  | 3   | 1           |       | 284  |
|                                    | 20 |   |       |      |      |      | 1    | 11  | 19  | 24  | 19 | 4   | 7  | 1   |             |       | 86   |
|                                    | 22 |   |       |      |      |      |      |     |     | 3   | 3  | 10  | 2  |     |             |       | 18   |
|                                    | 24 |   |       |      |      |      |      | 1   |     |     | 1  |     | 1  | 2   |             |       | 5    |
|                                    | 26 |   |       |      |      |      |      |     |     |     |    |     |    |     | 1           |       | 1    |
| Grand Total                        |    | 5870  | 11120 | 7914 | 4673 | 2594 | 1393 | 788 | 361 | 197 | 90 | 34  | 18 | 7   | 1           | 35060 |      |

| Summer                             |    | significant wave height, Hs [m] - upper lim |      |      |     |     |     |     |    |     |   |     |   |     | Grand Total |      |      |
|------------------------------------|----|---|------|------|-----|-----|-----|-----|----|-----|---|-----|---|-----|-------------|------|------|
|                                    |    | 0.5   | 1    | 1.5  | 2   | 2.5 | 3   | 3.5 | 4  | 4.5 | 5 | 5.5 | 6 | 6.5 |             | 7    |      |
| wind speed, Vw [m/s] - upper limit | 2  | 272   | 120  | 22   | 1   |     |     |     |    |     |   |     |   |     |             |      | 415  |
|                                    | 4  | 980   | 696  | 124  | 7   |     |     | 1   |    |     |   |     |   |     |             |      | 1808 |
|                                    | 6  | 867   | 1099 | 371  | 34  | 3   | 2   |     |    |     |   |     |   |     |             |      | 2376 |
|                                    | 8  | 220   | 967  | 595  | 147 | 10  | 2   | 2   |    |     |   |     |   |     |             |      | 1943 |
|                                    | 10 | 30  | 316  | 580  | 301 | 53  | 3   | 2   |    |     |   |     |   |     |             |      | 1285 |
|                                    | 12 |   | 26   | 211  | 282 | 125 | 24  | 3   | 1  |     |   |     |   |     |             |      | 672  |
|                                    | 14 |   |      | 6    | 49  | 126 | 48  | 28  | 8  |     |   |     |   |     |             |      | 265  |
|                                    | 16 |   |      |      | 1   | 8   | 27  | 14  | 2  | 1   |   |     |   |     |             |      | 53   |
|                                    | 18 |   |      |      |     | 1   | 5   | 4   | 3  |     |   |     |   |     |             |      | 13   |
|                                    | 20 |   |      |      |     |     |     |     |    |     |   |     |   |     |             |      |      |
|                                    | 22 |   |      |      |     |     |     |     |    |     |   |     |   |     |             |      |      |
|                                    | 24 |   |      |      |     |     |     |     |    |     |   |     |   |     |             |      |      |
|                                    | 26 |   |      |      |     |     |     |     |    |     |   |     |   |     |             |      |      |
| Grand Total                        |    | 2369  | 3224 | 1909 | 822 | 326 | 111 | 54  | 14 | 1   |   |     |   |     |             | 8830 |      |



## Annex C: Weibull parameters weather windows

The calculated Weibull parameters of the CDF for the duration and the number of low and high intervals and the probability  $P_{low}$  are given in Table C.2 - Table C.6 for the weather windows specified in Table C.1.

Table C.1: *Overview of weather windows*

| Weather window number | $H_{s,max}$ | $V_{w,max}$ | Weather window number | $H_{s,max}$ | $V_{w,max}$ |
|-----------------------|-------------|-------------|-----------------------|-------------|-------------|
|                       | [m]         | [m/s]       |                       | [m]         | [m/s]       |
| 1                     | 0.75        | 6           | 16                    | 2           | 15          |
| 2                     | 0.75        | 8           | 17                    | 3           | 8           |
| 3                     | 0.75        | 10          | 18                    | 3           | 10          |
| 4                     | 1           | 6           | 19                    | 3           | 12          |
| 5                     | 1           | 8           | 20                    | 3           | 15          |
| 6                     | 1           | 10          | 21                    | 3           | 20          |
| 7                     | 1           | 12          | 22                    | 4           | 12          |
| 8                     | 1.5         | 6           | 23                    | 4           | 15          |
| 9                     | 1.5         | 8           | 24                    | 4           | 20          |
| 10                    | 1.5         | 10          | 25                    | 4           | 30          |
| 11                    | 1.5         | 12          | 26                    | 5           | 15          |
| 12                    | 2           | 6           | 27                    | 5           | 20          |
| 13                    | 2           | 8           | 28                    | 5           | 30          |
| 14                    | 2           | 10          | 29                    | 8           | 20          |
| 15                    | 2           | 12          | 30                    | 8           | 30          |

Table C.2: *Weibull parameters of the CDF for the duration and the number of low and high intervals and the probability  $P_{low}$  for the winter period*

| WINTER |                    |                      |                  | Low intervals   |                 |                 |                 | High intervals  |                 |                 |                 |
|--------|--------------------|----------------------|------------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|
| Nr     | $H_{s,max}$<br>[m] | $V_{w,max}$<br>[m/s] | $P_{low}$<br>[%] | duration        |                 | number          |                 | duration        |                 | number          |                 |
|        |                    |                      |                  | $\alpha$<br>[-] | $\beta$<br>[hr] | $\alpha$<br>[-] | $\beta$<br>[hr] | $\alpha$<br>[-] | $\beta$<br>[hr] | $\alpha$<br>[-] | $\beta$<br>[hr] |
| 1      | 0.75               | 6                    | 19.7%            | 1.1391          | 62.458          | 0.62875         | 14.515          | 1.1048          | 358.46          | 0.53700         | 51.469          |
| 2      | 0.75               | 8                    | 21.7%            | 1.2755          | 66.906          | 0.67849         | 19.056          | 1.1342          | 339.00          | 0.57950         | 59.394          |
| 3      | 0.75               | 10                   | 21.8%            | 1.2757          | 67.264          | 0.68480         | 19.397          | 1.1305          | 336.50          | 0.58807         | 60.177          |
| 4      | 1                  | 6                    | 27.6%            | 1.0938          | 66.179          | 0.62922         | 14.381          | 1.0771          | 220.01          | 0.56144         | 34.060          |
| 5      | 1                  | 8                    | 33.3%            | 1.1633          | 86.053          | 0.65980         | 20.806          | 1.1199          | 203.78          | 0.60692         | 39.097          |
| 6      | 1                  | 10                   | 34.2%            | 1.1174          | 96.232          | 0.66071         | 21.927          | 1.1805          | 197.16          | 0.63687         | 43.450          |
| 7      | 1                  | 12                   | 34.3%            | 1.1305          | 96.888          | 0.65471         | 21.996          | 1.1814          | 197.18          | 0.63896         | 43.680          |
| 8      | 1.5                | 6                    | 35.2%            | 1.0008          | 65.086          | 0.63830         | 13.497          | 1.1366          | 126.24          | 0.61898         | 25.802          |
| 9      | 1.5                | 8                    | 48.9%            | 1.0323          | 116.32          | 0.60404         | 20.976          | 1.2327          | 103.37          | 0.65593         | 25.692          |
| 10     | 1.5                | 10                   | 55.2%            | 0.92679         | 169.51          | 0.60767         | 25.914          | 1.3473          | 91.249          | 0.73034         | 28.474          |
| 11     | 1.5                | 12                   | 56.2%            | 0.90733         | 181.76          | 0.61029         | 26.771          | 1.3142          | 90.202          | 0.75194         | 28.724          |
| 12     | 2                  | 6                    | 36.8%            | 0.98818         | 63.346          | 0.63746         | 13.012          | 1.1274          | 108.09          | 0.65024         | 24.510          |
| 13     | 2                  | 8                    | 54.2%            | 1.0451          | 114.21          | 0.56521         | 18.194          | 1.1853          | 73.069          | 0.6954          | 19.655          |
| 14     | 2                  | 10                   | 67.2%            | 1.0002          | 181.18          | 0.56708         | 26.347          | 1.2766          | 55.387          | 0.74575         | 17.790          |
| 15     | 2                  | 12                   | 72.9%            | 1.0115          | 230.88          | 0.58872         | 35.341          | 1.3563          | 48.955          | 0.83567         | 18.772          |
| 16     | 2                  | 15                   | 74.2%            | 1.0272          | 242.68          | 0.57767         | 36.816          | 1.2974          | 47.900          | 0.84989         | 18.355          |
| 17     | 3                  | 8                    | 55.3%            | 1.0326          | 113.83          | 0.54634         | 16.616          | 1.2660          | 62.076          | 0.7262          | 18.672          |
| 18     | 3                  | 10                   | 71.5%            | 0.99459         | 183.18          | 0.53497         | 23.127          | 1.3453          | 38.545          | 0.78885         | 14.031          |
| 19     | 3                  | 12                   | 83.4%            | 1.0234          | 302.55          | 0.50162         | 32.051          | 1.3007          | 25.529          | 0.85939         | 10.463          |
| 20     | 3                  | 15                   | 91.3%            | 0.97594         | 582.59          | 0.55004         | 65.089          | 1.3962          | 21.848          | 0.90054         | 9.8686          |
| 21     | 3                  | 20                   | 92.0%            | 1.0060          | 637.70          | 0.52044         | 67.245          | 1.3607          | 22.328          | 0.8482          | 9.4015          |
| 22     | 4                  | 12                   | 84.5%            | 1.0268          | 305.33          | 0.50153         | 32.428          | 1.3256          | 22.799          | 0.87639         | 9.7045          |
| 23     | 4                  | 15                   | 95.4%            | 1.0503          | 769.51          | 0.53738         | 87.035          | 1.1925          | 14.500          | 0.79263         | 5.6746          |
| 24     | 4                  | 20                   | 97.8%            | 1.5514          | 1468.6          | 0.41175         | 212.94          | 1.2414          | 18.224          | 0.77433         | 6.8453          |
| 25     | 4                  | 30                   | 97.8%            | 1.5514          | 1468.5          | 0.42155         | 222.79          | 1.2577          | 18.393          | 0.76604         | 6.8835          |
| 26     | 5                  | 15                   | 96.1%            | 1.0432          | 799.91          | 0.56827         | 96.555          | 1.2056          | 12.065          | 0.85434         | 5.2727          |
| 27     | 5                  | 20                   | 99.7%            | 3.4045          | 8692.1          | 0.50093         | 1495.4          | 1.7930          | 12.741          | 1.0740          | 7.5706          |
| 28     | 5                  | 30                   | 100.0%           |                 |                 |                 |                 |                 |                 |                 |                 |
| 29     | 8                  | 20                   | 100.0%           |                 |                 |                 |                 |                 |                 |                 |                 |
| 30     | 8                  | 30                   | 100.0%           |                 |                 |                 |                 |                 |                 |                 |                 |

Table C.3: Weibull parameters of the CDF for the duration and the number of low and high intervals and the probability  $P_{low}$  for the spring period

| SPRING |                    |                      |                  | Low intervals   |                 |                 |                 | High intervals  |                 |                 |                 |
|--------|--------------------|----------------------|------------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|
| Nr     | $H_{s,max}$<br>[m] | $V_{w,max}$<br>[m/s] | $P_{low}$<br>[%] | duration        |                 | number          |                 | duration        |                 | number          |                 |
|        |                    |                      |                  | $\alpha$<br>[-] | $\beta$<br>[hr] | $\alpha$<br>[-] | $\beta$<br>[hr] | $\alpha$<br>[-] | $\beta$<br>[hr] | $\alpha$<br>[-] | $\beta$<br>[hr] |
| 1      | 0.75               | 6                    | 30.3%            | 1.0977          | 42.332          | 0.80666         | 14.091          | 1.1619          | 154.30          | 0.52317         | 23.047          |
| 2      | 0.75               | 8                    | 37.1%            | 1.2912          | 66.887          | 0.73009         | 20.676          | 1.2671          | 146.88          | 0.56060         | 27.625          |
| 3      | 0.75               | 10                   | 38.5%            | 1.1884          | 84.260          | 0.71124         | 23.271          | 1.2912          | 149.26          | 0.60702         | 33.227          |
| 4      | 1                  | 6                    | 38.7%            | 1.0934          | 44.198          | 0.79014         | 14.325          | 1.1524          | 98.898          | 0.56594         | 17.651          |
| 5      | 1                  | 8                    | 52.0%            | 1.3219          | 86.818          | 0.67667         | 23.949          | 1.1556          | 95.424          | 0.56994         | 17.944          |
| 6      | 1                  | 10                   | 55.3%            | 1.2286          | 126.79          | 0.64724         | 30.497          | 1.1956          | 98.063          | 0.65984         | 24.345          |
| 7      | 1                  | 12                   | 55.6%            | 1.2258          | 130.61          | 0.65511         | 31.909          | 1.2005          | 98.647          | 0.67266         | 25.277          |
| 8      | 1.5                | 6                    | 45.5%            | 1.1501          | 44.163          | 0.75847         | 14.088          | 1.1230          | 66.548          | 0.61909         | 14.160          |
| 9      | 1.5                | 8                    | 66.0%            | 1.3395          | 99.565          | 0.66313         | 26.353          | 1.0654          | 50.779          | 0.64329         | 11.702          |
| 10     | 1.5                | 10                   | 75.7%            | 1.3054          | 197.37          | 0.63774         | 48.472          | 1.1424          | 51.658          | 0.7544          | 15.838          |
| 11     | 1.5                | 12                   | 77.3%            | 1.3520          | 241.56          | 0.63323         | 61.196          | 1.1763          | 54.056          | 0.85255         | 19.244          |
| 12     | 2                  | 6                    | 46.7%            | 1.1416          | 44.082          | 0.75985         | 14.052          | 1.1526          | 60.285          | 0.63743         | 13.971          |
| 13     | 2                  | 8                    | 69.5%            | 1.3224          | 104.52          | 0.64072         | 25.580          | 1.1741          | 37.790          | 0.69946         | 10.92           |
| 14     | 2                  | 10                   | 82.9%            | 1.2651          | 239.90          | 0.58255         | 48.274          | 1.0681          | 33.354          | 0.80262         | 11.007          |
| 15     | 2                  | 12                   | 87.3%            | 1.3039          | 383.63          | 0.53714         | 68.277          | 1.1199          | 35.386          | 0.77920         | 11.406          |
| 16     | 2                  | 15                   | 87.9%            | 1.2017          | 446.49          | 0.54362         | 74.950          | 1.1458          | 37.041          | 0.79560         | 12.364          |
| 17     | 3                  | 8                    | 70.6%            | 1.3192          | 104.87          | 0.63575         | 25.225          | 1.2443          | 33.394          | 0.72754         | 10.722          |
| 18     | 3                  | 10                   | 85.4%            | 1.2495          | 245.95          | 0.54424         | 42.580          | 1.1398          | 22.202          | 0.90769         | 9.2395          |
| 19     | 3                  | 12                   | 93.4%            | 1.2071          | 565.43          | 0.48864         | 71.432          | 1.1581          | 17.597          | 0.81730         | 6.8725          |
| 20     | 3                  | 15                   | 96.0%            | 1.2581          | 890.93          | 0.49653         | 126.46          | 1.6648          | 15.590          | 1.0066          | 8.4253          |
| 21     | 3                  | 20                   | 96.4%            | 1.1819          | 1027.4          | 0.50074         | 137.51          | 1.5846          | 15.734          | 0.97082         | 8.1514          |
| 22     | 4                  | 12                   | 93.9%            | 1.2172          | 597.01          | 0.47958         | 70.806          | 1.1671          | 15.580          | 0.86567         | 6.5663          |
| 23     | 4                  | 15                   | 97.8%            | 1.1269          | 1326.6          | 0.55549         | 169.05          | 1.6815          | 10.052          | 1.0691          | 5.9752          |
| 24     | 4                  | 20                   | 98.8%            | 1.7779          | 1296.3          | 0.72420         | 527.79          | 2.1706          | 8.8823          | 1.4565          | 6.4690          |
| 25     | 4                  | 30                   | 98.9%            | 1.7746          | 1296.4          | 0.72580         | 526.97          | 2.1380          | 8.9686          | 1.3049          | 6.2151          |
| 26     | 5                  | 15                   | 98.1%            | 1.0153          | 1557.8          | 0.59635         | 182.49          | 1.5006          | 9.7827          | 1.0237          | 5.5323          |
| 27     | 5                  | 20                   | 100.0%           |                 |                 |                 |                 |                 |                 |                 |                 |
| 28     | 5                  | 30                   | 100.0%           |                 |                 |                 |                 |                 |                 |                 |                 |
| 29     | 8                  | 20                   | 100.0%           |                 |                 |                 |                 |                 |                 |                 |                 |
| 30     | 8                  | 30                   | 100.0%           |                 |                 |                 |                 |                 |                 |                 |                 |

Table C.4: Weibull parameters of the CDF for the duration and the number of low and high intervals and the probability  $P_{low}$  for the summer period

| SUMMER |                    |                      |                  | Low intervals   |                 |                 |                 | High intervals  |                 |                 |                 |
|--------|--------------------|----------------------|------------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|
| Nr     | $H_{s,max}$<br>[m] | $V_{w,max}$<br>[m/s] | $P_{low}$<br>[%] | duration        |                 | number          |                 | duration        |                 | number          |                 |
|        |                    |                      |                  | $\alpha$<br>[-] | $\beta$<br>[hr] | $\alpha$<br>[-] | $\beta$<br>[hr] | $\alpha$<br>[-] | $\beta$<br>[hr] | $\alpha$<br>[-] | $\beta$<br>[hr] |
| 1      | 0.75               | 6                    | 38.8%            | 1.3481          | 46.127          | 0.82877         | 17.532          | 1.2378          | 109.44          | 0.56224         | 20.761          |
| 2      | 0.75               | 8                    | 46.4%            | 1.2918          | 87.173          | 0.71924         | 26.150          | 1.3214          | 108.98          | 0.64585         | 28.537          |
| 3      | 0.75               | 10                   | 47.7%            | 1.2269          | 103.31          | 0.71185         | 29.026          | 1.3434          | 109.72          | 0.70382         | 33.050          |
| 4      | 1                  | 6                    | 47.2%            | 1.2974          | 47.483          | 0.77409         | 16.341          | 1.1704          | 67.323          | 0.62394         | 15.314          |
| 5      | 1                  | 8                    | 59.8%            | 1.2138          | 100.65          | 0.70981         | 28.282          | 1.2476          | 67.612          | 0.65137         | 17.419          |
| 6      | 1                  | 10                   | 64.0%            | 1.2470          | 148.21          | 0.68387         | 39.285          | 1.2980          | 70.503          | 0.76852         | 23.676          |
| 7      | 1                  | 12                   | 64.2%            | 1.2438          | 154.57          | 0.67295         | 39.914          | 1.3036          | 70.740          | 0.77908         | 24.242          |
| 8      | 1.5                | 6                    | 52.7%            | 1.2916          | 47.628          | 0.77884         | 16.388          | 1.1341          | 47.456          | 0.70626         | 13.319          |
| 9      | 1.5                | 8                    | 72.1%            | 1.1947          | 110.57          | 0.69319         | 29.630          | 1.1778          | 37.183          | 0.68814         | 10.566          |
| 10     | 1.5                | 10                   | 83.2%            | 1.3693          | 250.97          | 0.59720         | 57.875          | 1.2261          | 36.487          | 0.79834         | 13.000          |
| 11     | 1.5                | 12                   | 85.7%            | 1.3242          | 347.13          | 0.55096         | 67.021          | 1.3362          | 36.947          | 0.81704         | 14.041          |
| 12     | 2                  | 6                    | 53.0%            | 1.2906          | 47.464          | 0.76994         | 16.113          | 1.1471          | 45.503          | 0.71640         | 13.174          |
| 13     | 2                  | 8                    | 74.0%            | 1.1862          | 111.14          | 0.68087         | 28.957          | 1.1106          | 31.989          | 0.70940         | 9.3961          |
| 14     | 2                  | 10                   | 88.6%            | 1.3053          | 311.82          | 0.54063         | 57.169          | 1.0864          | 26.305          | 0.69923         | 7.7655          |
| 15     | 2                  | 12                   | 94.2%            | 1.5523          | 624.89          | 0.50246         | 122.97          | 1.2008          | 24.460          | 0.75172         | 8.5239          |
| 16     | 2                  | 15                   | 94.8%            | 1.5395          | 748.00          | 0.49522         | 139.28          | 1.1843          | 24.750          | 0.80382         | 9.1413          |
| 17     | 3                  | 8                    | 74.2%            | 1.1934          | 111.40          | 0.67676         | 28.784          | 1.1294          | 30.957          | 0.72129         | 9.4364          |
| 18     | 3                  | 10                   | 89.5%            | 1.2634          | 339.21          | 0.52237         | 56.543          | 1.1236          | 23.078          | 0.72925         | 7.5175          |
| 19     | 3                  | 12                   | 96.5%            | 2.1183          | 686.82          | 0.48286         | 165.25          | 1.5367          | 13.419          | 0.97566         | 7.0559          |
| 20     | 3                  | 15                   | 99.1%            | 1.6426          | 1964.3          | 0.75140         | 810.32          | 1.9819          | 9.8907          | 1.1749          | 6.3990          |
| 21     | 3                  | 20                   | 99.2%            | 1.9935          | 2166.2          | 0.73143         | 1058.8          | 2.4335          | 10.803          | 1.3843          | 7.8001          |
| 22     | 4                  | 12                   | 96.6%            | 1.9682          | 711.90          | 0.46347         | 155.14          | 1.4672          | 13.026          | 0.96844         | 6.7305          |
| 23     | 4                  | 15                   | 99.6%            | 1.8043          | 2621.3          | 0.76868         | 1183.7          | 1.4123          | 5.4989          | 0.98159         | 3.2105          |
| 24     | 4                  | 20                   | 100.0%           |                 |                 |                 |                 |                 |                 |                 |                 |
| 25     | 4                  | 30                   | 100.0%           |                 |                 |                 |                 |                 |                 |                 |                 |
| 26     | 5                  | 15                   | 99.7%            | 2.0797          | 2767.7          | 0.81607         | 1370            | 1.4667          | 5.6487          | 1.0141          | 3.3769          |
| 27     | 5                  | 20                   | 100.0%           |                 |                 |                 |                 |                 |                 |                 |                 |
| 28     | 5                  | 30                   | 100.0%           |                 |                 |                 |                 |                 |                 |                 |                 |
| 29     | 8                  | 20                   | 100.0%           |                 |                 |                 |                 |                 |                 |                 |                 |
| 30     | 8                  | 30                   | 100.0%           |                 |                 |                 |                 |                 |                 |                 |                 |

Table C.5: Weibull parameters of the CDF for the duration and the number of low and high intervals and the probability  $P_{low}$  for the autumn period

| AUTUMN |                    |                      |                  | Low intervals   |                 |                 |                 | High intervals  |                 |                 |                 |
|--------|--------------------|----------------------|------------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|
| Nr     | $H_{s,max}$<br>[m] | $V_{w,max}$<br>[m/s] | $P_{low}$<br>[%] | duration        |                 | number          |                 | duration        |                 | number          |                 |
|        |                    |                      |                  | $\alpha$<br>[-] | $\beta$<br>[hr] | $\alpha$<br>[-] | $\beta$<br>[hr] | $\alpha$<br>[-] | $\beta$<br>[hr] | $\alpha$<br>[-] | $\beta$<br>[hr] |
| 1      | 0.75               | 6                    | 23.1%            | 1.2420          | 42.390          | 0.75577         | 13.810          | 1.2050          | 228.43          | 0.51851         | 33.711          |
| 2      | 0.75               | 8                    | 25.5%            | 1.1590          | 59.470          | 0.74458         | 17.619          | 1.2288          | 230.65          | 0.58471         | 44.717          |
| 3      | 0.75               | 10                   | 25.6%            | 1.1113          | 61.630          | 0.74931         | 17.840          | 1.2327          | 230.80          | 0.59030         | 45.679          |
| 4      | 1                  | 6                    | 33.0%            | 1.2709          | 46.841          | 0.77664         | 15.901          | 1.3009          | 136.51          | 0.55012         | 25.265          |
| 5      | 1                  | 8                    | 39.9%            | 1.2532          | 83.471          | 0.71957         | 24.698          | 1.3253          | 137.95          | 0.65703         | 36.124          |
| 6      | 1                  | 10                   | 41.6%            | 1.1084          | 99.872          | 0.69395         | 24.982          | 1.2957          | 136.80          | 0.68107         | 37.229          |
| 7      | 1                  | 12                   | 41.6%            | 1.0841          | 102.00          | 0.68900         | 24.754          | 1.2961          | 136.44          | 0.68216         | 37.179          |
| 8      | 1.5                | 6                    | 41.9%            | 1.2767          | 47.695          | 0.73649         | 15.048          | 1.2384          | 81.040          | 0.62502         | 18.548          |
| 9      | 1.5                | 8                    | 57.3%            | 1.2451          | 105.09          | 0.64884         | 25.992          | 1.2250          | 72.913          | 0.70140         | 20.109          |
| 10     | 1.5                | 10                   | 64.5%            | 1.1860          | 154.32          | 0.63487         | 34.747          | 1.2519          | 71.189          | 0.72615         | 20.844          |
| 11     | 1.5                | 12                   | 65.6%            | 1.1273          | 172.18          | 0.63763         | 36.514          | 1.2726          | 72.265          | 0.73040         | 21.530          |
| 12     | 2                  | 6                    | 44.0%            | 1.2238          | 47.297          | 0.74198         | 14.736          | 1.1361          | 71.887          | 0.65591         | 17.206          |
| 13     | 2                  | 8                    | 62.9%            | 1.1442          | 109.71          | 0.63309         | 24.175          | 1.0757          | 55.212          | 0.72594         | 15.197          |
| 14     | 2                  | 10                   | 75.2%            | 1.1623          | 208.96          | 0.56353         | 35.709          | 1.1722          | 46.904          | 0.74041         | 14.183          |
| 15     | 2                  | 12                   | 80.2%            | 1.1988          | 315.20          | 0.55302         | 52.857          | 1.3095          | 47.254          | 0.82179         | 17.511          |
| 16     | 2                  | 15                   | 80.7%            | 1.2130          | 343.36          | 0.53594         | 54.259          | 1.3359          | 47.825          | 0.84359         | 18.457          |
| 17     | 3                  | 8                    | 64.5%            | 1.1350          | 108.53          | 0.63484         | 23.747          | 1.0374          | 51.742          | 0.71083         | 13.535          |
| 18     | 3                  | 10                   | 79.4%            | 1.1851          | 210.20          | 0.55902         | 35.975          | 1.0525          | 35.640          | 0.77435         | 11.072          |
| 19     | 3                  | 12                   | 89.5%            | 1.1137          | 464.10          | 0.52386         | 59.789          | 1.1620          | 25.713          | 0.88022         | 10.199          |
| 20     | 3                  | 15                   | 94.9%            | 1.1939          | 936.75          | 0.53173         | 145.67          | 1.1269          | 28.092          | 0.89718         | 10.734          |
| 21     | 3                  | 20                   | 95.8%            | 1.0667          | 1400.2          | 0.51234         | 159.02          | 1.1155          | 29.237          | 0.88855         | 11.019          |
| 22     | 4                  | 12                   | 90.6%            | 1.1408          | 482.92          | 0.50621         | 59.330          | 1.2257          | 22.269          | 0.89764         | 9.4577          |
| 23     | 4                  | 15                   | 97.8%            | 1.1987          | 1557.0          | 0.45048         | 207.10          | 1.0992          | 16.265          | 0.92806         | 6.8235          |
| 24     | 4                  | 20                   | 99.5%            | 2.8142          | 5333.0          | 0.29499         | 530.91          | 1.3356          | 12.262          | 0.89636         | 5.7529          |
| 25     | 4                  | 30                   | 99.5%            | 2.8171          | 5332.2          | 0.30405         | 579.88          | 1.3588          | 12.359          | 0.91602         | 5.9243          |
| 26     | 5                  | 15                   | 98.1%            | 1.2418          | 1645.7          | 0.45242         | 243.23          | 1.0645          | 15.486          | 0.84801         | 5.8758          |
| 27     | 5                  | 20                   | 99.9%            | 11.917          | 7056.1          | 1.9238          | 6318.0          | 1.2540          | 6.4261          | 0.79413         | 2.7200          |
| 28     | 5                  | 30                   | 100.0%           |                 |                 |                 |                 |                 |                 |                 |                 |
| 29     | 8                  | 20                   | 100.0%           |                 |                 |                 |                 |                 |                 |                 |                 |
| 30     | 8                  | 30                   | 100.0%           |                 |                 |                 |                 |                 |                 |                 |                 |

Table C.6: Weibull parameters of the CDF for the duration and the number of low and high intervals and the probability  $P_{low}$  for the whole year

| YEAR |                    |                      |                  | Low intervals   |                 |                 |                 | High intervals  |                 |                 |                 |
|------|--------------------|----------------------|------------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|
| Nr   | $H_{s,max}$<br>[m] | $V_{w,max}$<br>[m/s] | $P_{low}$<br>[%] | duration        |                 | number          |                 | duration        |                 | number          |                 |
|      |                    |                      |                  | $\alpha$<br>[-] | $\beta$<br>[hr] | $\alpha$<br>[-] | $\beta$<br>[hr] | $\alpha$<br>[-] | $\beta$<br>[hr] | $\alpha$<br>[-] | $\beta$<br>[hr] |
| 1    | 0.75               | 6                    | 28.1%            | 1.1707          | 46.978          | 0.7667          | 15.170          | 1.0173          | 206.67          | 0.53304         | 27.503          |
| 2    | 0.75               | 8                    | 32.8%            | 1.2172          | 72.661          | 0.71838         | 21.074          | 1.0498          | 205.54          | 0.58901         | 35.496          |
| 3    | 0.75               | 10                   | 33.5%            | 1.1467          | 83.913          | 0.70497         | 22.486          | 1.0580          | 207.08          | 0.61976         | 39.642          |
| 4    | 1                  | 6                    | 36.7%            | 1.1512          | 49.578          | 0.74963         | 15.309          | 1.0462          | 126.50          | 0.56716         | 20.322          |
| 5    | 1                  | 8                    | 46.3%            | 1.2260          | 90.510          | 0.69483         | 24.675          | 1.0699          | 127.90          | 0.60487         | 24.358          |
| 6    | 1                  | 10                   | 48.8%            | 1.1403          | 123.91          | 0.65849         | 28.847          | 1.0988          | 130.08          | 0.66912         | 30.303          |
| 7    | 1                  | 12                   | 49.0%            | 1.1397          | 127.38          | 0.65450         | 29.219          | 1.1023          | 130.39          | 0.67575         | 30.880          |
| 8    | 1.5                | 6                    | 43.9%            | 1.1491          | 49.629          | 0.73474         | 14.872          | 1.0594          | 79.328          | 0.62923         | 16.478          |
| 9    | 1.5                | 8                    | 61.1%            | 1.2062          | 107.33          | 0.65737         | 25.989          | 1.0604          | 68.657          | 0.64752         | 15.321          |
| 10   | 1.5                | 10                   | 69.7%            | 1.1651          | 200.06          | 0.60349         | 38.985          | 1.1566          | 68.443          | 0.71976         | 19.082          |
| 11   | 1.5                | 12                   | 71.3%            | 1.1261          | 246.01          | 0.58015         | 42.204          | 1.1726          | 69.683          | 0.75167         | 20.880          |
| 12   | 2                  | 6                    | 45.2%            | 1.1346          | 49.269          | 0.73235         | 14.598          | 1.0764          | 70.438          | 0.65296         | 16.045          |
| 13   | 2                  | 8                    | 65.2%            | 1.1842          | 109.59          | 0.63306         | 24.332          | 1.0543          | 51.002          | 0.68872         | 13.048          |
| 14   | 2                  | 10                   | 78.5%            | 1.1514          | 242.01          | 0.55382         | 38.574          | 1.1293          | 44.086          | 0.72220         | 12.743          |
| 15   | 2                  | 12                   | 83.8%            | 1.1565          | 403.49          | 0.52123         | 54.737          | 1.2336          | 43.429          | 0.78636         | 14.850          |
| 16   | 2                  | 15                   | 84.6%            | 1.0988          | 461.34          | 0.51361         | 57.123          | 1.2356          | 43.641          | 0.80992         | 15.492          |
| 17   | 3                  | 8                    | 66.2%            | 1.1807          | 109.35          | 0.62518         | 23.581          | 1.1025          | 45.725          | 0.70528         | 12.568          |
| 18   | 3                  | 10                   | 81.4%            | 1.1349          | 248.98          | 0.53172         | 35.592          | 1.1428          | 32.020          | 0.77480         | 10.670          |
| 19   | 3                  | 12                   | 90.6%            | 1.1833          | 527.11          | 0.46844         | 55.306          | 1.1926          | 22.856          | 0.85666         | 9.1187          |
| 20   | 3                  | 15                   | 95.4%            | 1.0608          | 1167.4          | 0.48096         | 115.37          | 1.2562          | 21.591          | 0.92232         | 9.4615          |
| 21   | 3                  | 20                   | 95.8%            | 1.0310          | 1432.6          | 0.46164         | 116.86          | 1.2498          | 22.362          | 0.89772         | 9.4859          |
| 22   | 4                  | 12                   | 91.3%            | 1.1850          | 544.54          | 0.46075         | 54.574          | 1.2235          | 20.386          | 0.87401         | 8.5336          |
| 23   | 4                  | 15                   | 97.6%            | 1.0728          | 1663.9          | 0.46417         | 155.44          | 1.1228          | 13.886          | 0.86216         | 5.8275          |
| 24   | 4                  | 20                   | 99.0%            | 1.1782          | 3998.5          | 0.38286         | 372.23          | 1.1897          | 14.716          | 0.86911         | 6.2930          |
| 25   | 4                  | 30                   | 99.0%            | 1.1800          | 3991.9          | 0.39266         | 391.74          | 1.1989          | 14.877          | 0.85907         | 6.3111          |
| 26   | 5                  | 15                   | 98.0%            | 1.0629          | 1826.2          | 0.47750         | 175.21          | 1.1388          | 12.253          | 0.87572         | 5.2961          |
| 27   | 5                  | 20                   | 99.8%            | 2.3480          | 8909.6          | 0.51396         | 2385.7          | 1.5255          | 11.644          | 0.90364         | 5.9140          |
| 28   | 5                  | 30                   | 99.8%            | 1.4523          | 14844           | 0.50733         | 3080.6          | 2.2365          | 13.710          | 1.1173          | 8.6815          |
| 29   | 8                  | 20                   | 99.9%            | 2.0305          | 13604           | 0.53708         | 4467.5          | 1.9448          | 4.1807          | 1.5760          | 3.1724          |
| 30   | 8                  | 30                   | 100.0%           |                 |                 |                 |                 |                 |                 |                 |                 |



## Annex D: Time to wait results

The waiting time for a mission with duration of  $t$  hours is given by

$$T_{\text{wait}} = C_0 + C_1t + C_2t^2 + C_3t^3$$

For the weather windows specified in Table D.1 the polynomial coefficients  $C_i$ ,  $i = 0, \dots, 3$  are given in Table D.2.

Table D.1: *Overview of weather windows*

| Weather window number | $H_{s, \max}$<br>[m] | $V_{w, \max}$<br>[m/s] | Weather window number | $H_{s, \max}$<br>[m] | $V_{w, \max}$<br>[m/s] |
|-----------------------|----------------------|------------------------|-----------------------|----------------------|------------------------|
| 1                     | 0.75                 | 6                      | 16                    | 2                    | 15                     |
| 2                     | 0.75                 | 8                      | 17                    | 3                    | 8                      |
| 3                     | 0.75                 | 10                     | 18                    | 3                    | 10                     |
| 4                     | 1                    | 6                      | 19                    | 3                    | 12                     |
| 5                     | 1                    | 8                      | 20                    | 3                    | 15                     |
| 6                     | 1                    | 10                     | 21                    | 3                    | 20                     |
| 7                     | 1                    | 12                     | 22                    | 4                    | 12                     |
| 8                     | 1.5                  | 6                      | 23                    | 4                    | 15                     |
| 9                     | 1.5                  | 8                      | 24                    | 4                    | 20                     |
| 10                    | 1.5                  | 10                     | 25                    | 4                    | 30                     |
| 11                    | 1.5                  | 12                     | 26                    | 5                    | 15                     |
| 12                    | 2                    | 6                      | 27                    | 5                    | 20                     |
| 13                    | 2                    | 8                      | 28                    | 5                    | 30                     |
| 14                    | 2                    | 10                     | 29                    | 8                    | 20                     |
| 15                    | 2                    | 12                     | 30                    | 8                    | 30                     |

Table D.2: *Polynomial coefficients for waiting time*

| Winter             |                    |                         |                |                |                | Spring             |                    |                         |                |                |                | Summer             |                    |                         |                |                |                |
|--------------------|--------------------|-------------------------|----------------|----------------|----------------|--------------------|--------------------|-------------------------|----------------|----------------|----------------|--------------------|--------------------|-------------------------|----------------|----------------|----------------|
| weather window     |                    | polynomial coefficients |                |                |                | weather window     |                    | polynomial coefficients |                |                |                | weather window     |                    | polynomial coefficients |                |                |                |
| H <sub>s,max</sub> | V <sub>w,max</sub> | C <sub>0</sub>          | C <sub>1</sub> | C <sub>2</sub> | C <sub>3</sub> | H <sub>s,max</sub> | V <sub>w,max</sub> | C <sub>0</sub>          | C <sub>1</sub> | C <sub>2</sub> | C <sub>3</sub> | H <sub>s,max</sub> | V <sub>w,max</sub> | C <sub>0</sub>          | C <sub>1</sub> | C <sub>2</sub> | C <sub>3</sub> |
| 0.75               | 6                  | 127.836                 | 13.35595       | -0.125518      | 0.004006       | 0.75               | 6                  | 41.52782                | 5.899317       | -0.013608      | 0.005202       | 0.75               | 6                  | 28.74454                | 3.635979       | 0.006345       | 0.002946       |
| 0.75               | 8                  | 116.5792                | 10.75958       | -0.146188      | 0.003692       | 0.75               | 8                  | 37.24326                | 3.915248       | -0.010349      | 0.001654       | 0.75               | 8                  | 23.17037                | 3.750624       | -0.05864       | 0.001406       |
| 0.75               | 10                 | 108.7434                | 10.00367       | -0.090582      | 0.002693       | 0.75               | 10                 | 39.24181                | 2.094214       | 0.082962       | 5.44E-05       | 0.75               | 10                 | 20.37167                | 3.03021        | -0.020759      | 0.000806       |
| 1                  | 6                  | 90.75643                | 3.950768       | 0.140226       | 0.000628       | 1                  | 6                  | 34.16386                | 1.657042       | 0.118821       | 0.001942       | 1                  | 6                  | 15.19936                | 3.201289       | -0.028375      | 0.002174       |
| 1                  | 8                  | 69.07969                | 3.544768       | 0.087804       | 0.000116       | 1                  | 8                  | 21.04359                | 2.05153        | 0.005328       | 0.000491       | 1                  | 8                  | 9.471205                | 0.971495       | 0.024888       | 0.0002         |
| 1                  | 10                 | 71.52711                | 1.458832       | 0.114669       | 0              | 1                  | 10                 | 18.09406                | 1.386803       | 0.004772       | 0.000283       | 1                  | 10                 | 8.463008                | 1.090568       | 0.006987       | 0.000141       |
| 1                  | 12                 | 65.20972                | 1.778173       | 0.101413       | 0              | 1                  | 12                 | 21.29345                | 0.3671         | 0.040344       | 0              | 1                  | 12                 | 7.445337                | 1.244904       | -0.001747      | 0.000177       |
| 1.5                | 6                  | 49.13868                | 2.240212       | 0.139067       | 0              | 1.5                | 6                  | 14.78555                | 3.18474        | -0.017913      | 0.002961       | 1.5                | 6                  | 8.219994                | 2.209574       | -0.007681      | 0.001924       |
| 1.5                | 8                  | 23.33379                | 1.748556       | 0.051853       | 0              | 1.5                | 8                  | 11.05083                | 0.353914       | 0.035119       | 6.18E-06       | 1.5                | 8                  | 3.559139                | 0.654996       | 0.016793       | 0.000141       |
| 1.5                | 10                 | 25.5843                 | 0.550888       | 0.042377       | 0              | 1.5                | 10                 | 7.313341                | 0.465182       | 0.006091       | 5.71E-05       | 1.5                | 10                 | 1.982866                | 0.289328       | 0.006946       | 1.51E-05       |
| 1.5                | 12                 | 24.16063                | 0.793979       | 0.035555       | 0              | 1.5                | 12                 | 6.533664                | 0.556066       | 0.00422        | 4.62E-05       | 1.5                | 12                 | 1.372772                | 0.466275       | -0.000617      | 3.54E-05       |
| 2                  | 6                  | 43.42893                | 2.091328       | 0.130862       | 0              | 2                  | 6                  | 11.0353                 | 2.325534       | 0.030973       | 0.002285       | 2                  | 6                  | 3.003118                | 2.97946        | -0.038369      | 0.002149       |
| 2                  | 8                  | 11.80419                | 2.263339       | 0.033966       | 0              | 2                  | 8                  | 6.124716                | 0.278781       | 0.033652       | 0              | 2                  | 8                  | 2.446146                | 0.496041       | 0.024987       | 4.77E-05       |
| 2                  | 10                 | 6.150373                | 0.624626       | 0.024282       | 0              | 2                  | 10                 | 4.194705                | 0.121287       | 0.011694       | 0              | 2                  | 10                 | 1.244981                | 0.162984       | 0.006647       | 3.02E-06       |
| 2                  | 12                 | 10.64462                | 0.209222       | 0.019331       | 0              | 2                  | 12                 | 2.194576                | 0.067626       | 0.007511       | 0              | 2                  | 12                 | 0.911289                | 0.017303       | 0.001356       | 9.7E-06        |
| 2                  | 15                 | 10.13819                | 0.04213        | 0.018179       | 0              | 2                  | 15                 | 1.682272                | 0.043262       | 0.006568       | 0              | 2                  | 15                 | 0                       | 0.046441       | 0.001661       | 2.73E-06       |
| 3                  | 8                  | 13.71656                | 1.540357       | 0.035554       | 1.55E-05       | 3                  | 8                  | 6.504572                | 0.183829       | 0.035057       | 0              | 3                  | 8                  | 0                       | 0.144084       | 0.033719       | 0              |
| 3                  | 10                 | 3.999631                | 1.158457       | 0.003601       | 0.000113       | 3                  | 10                 | 0.772581                | 0.159586       | 0.009513       | 0              | 3                  | 10                 | 0                       | 0.299664       | 0.004544       | 0              |
| 3                  | 12                 | 0                       | 0.679058       | 0.000677       | 5.22E-05       | 3                  | 12                 | 0                       | 0.020711       | 0.00397        | 3.32E-06       | 3                  | 12                 | 0                       | 0.068018       | 0.002028       | 0              |
| 3                  | 15                 | 0                       | 0.206504       | 0.004351       | 0              | 3                  | 15                 | 0                       | 0.023446       | 0.001365       | 5.28E-06       | 3                  | 15                 | 0                       | 0.106364       | 0.000362       | 0              |
| 3                  | 20                 | 0                       | 0.013042       | 0.006164       | 0              | 3                  | 20                 | 0                       | 0.10038        | 0.000848       | 0              | 3                  | 20                 | 0                       | 0.034981       | 0.000299       | 0              |
| 4                  | 12                 | 0                       | 0.238412       | 0.00965        | 0              | 4                  | 12                 | 0                       | 0.005278       | 0.004266       | 2.16E-06       | 4                  | 12                 | 0                       | 0.01016        | 0.002179       | 0              |
| 4                  | 15                 | 0                       | 0.213714       | -0.002399      | 3.15E-05       | 4                  | 15                 | 0                       | 0.041309       | 0.0005         | 6.22E-06       | 4                  | 15                 | 0                       | 0.072709       | -7.6E-05       | 1.09E-06       |
| 4                  | 20                 | 0                       | 0.066647       | -0.000164      | 9.35E-06       | 4                  | 20                 | 0                       | 0.044961       | -0.000107      | 6.94E-06       | 4                  | 20                 | 0                       | 0              | 0              | 0              |
| 4                  | 30                 | 0                       | 0.033317       | 0.001416       | 0              | 4                  | 30                 | 0                       | 0.091497       | -0.000837      | 1.17E-05       | 4                  | 30                 | 0                       | 0              | 0              | 0              |
| 5                  | 15                 | 0                       | 0.049676       | 0.00328        | 0              | 5                  | 15                 | 0                       | 0.060053       | 0.000379       | 7.89E-06       | 5                  | 15                 | 0                       | 0.017054       | 9.52E-05       | 6.63E-07       |
| 5                  | 20                 | 0                       | 0.027762       | -2.91E-05      | 3.91E-07       | 5                  | 20                 | 0                       | 0              | 0              | 0              | 5                  | 20                 | 0                       | 0              | 0              | 0              |
| 5                  | 30                 | 0                       | 0              | 0              | 0              | 5                  | 30                 | 0                       | 0              | 0              | 0              | 5                  | 30                 | 0                       | 0              | 0              | 0              |
| 8                  | 20                 | 0                       | 0              | 0              | 0              | 8                  | 20                 | 0                       | 0              | 0              | 0              | 8                  | 20                 | 0                       | 0              | 0              | 0              |
| 8                  | 30                 | 0                       | 0              | 0              | 0              | 8                  | 30                 | 0                       | 0              | 0              | 0              | 8                  | 30                 | 0                       | 0              | 0              | 0              |

Autumn

| weather window     |                    | polynomial coefficients |                |                |                |
|--------------------|--------------------|-------------------------|----------------|----------------|----------------|
| H <sub>s,max</sub> | V <sub>w,max</sub> | C <sub>0</sub>          | C <sub>1</sub> | C <sub>2</sub> | C <sub>3</sub> |
| 0.75               | 6                  | 104.7626                | 0.89863        | 0.418606       | 0              |
| 0.75               | 8                  | 99.53664                | 0.63713        | 0.284419       | 0              |
| 0.75               | 10                 | 96.54334                | 0.800418       | 0.28246        | 0              |
| 1                  | 6                  | 51.81158                | 1.433948       | 0.241665       | 0              |
| 1                  | 8                  | 47.0512                 | 1.334731       | 0.083931       | 0              |
| 1                  | 10                 | 44.07898                | 1.294558       | 0.08244        | 0              |
| 1                  | 12                 | 40.39507                | 1.695597       | 0.06924        | 0              |
| 1.5                | 6                  | 27.96359                | 0.574589       | 0.163773       | 0              |
| 1.5                | 8                  | 18.0074                 | 0.453196       | 0.042619       | 0              |
| 1.5                | 10                 | 15.04943                | 0.2885         | 0.030407       | 0              |
| 1.5                | 12                 | 12.45818                | 0.305154       | 0.0268         | 0              |
| 2                  | 6                  | 20.74555                | 0.590623       | 0.15756        | 0              |
| 2                  | 8                  | 16.05795                | 0.213348       | 0.039599       | 0              |
| 2                  | 10                 | 9.011325                | 0.215292       | 0.015411       | 0              |
| 2                  | 12                 | 3.975207                | 0.304786       | 0.009134       | 0              |
| 2                  | 15                 | 1.431014                | 0.397343       | 0.007081       | 0              |
| 3                  | 8                  | 11.10633                | 0.471226       | 0.037004       | 0              |
| 3                  | 10                 | 6.351079                | 0.163329       | 0.015278       | 0              |
| 3                  | 12                 | 0                       | 0.186681       | 0.005946       | 0              |
| 3                  | 15                 | 0                       | 0.091074       | 0.001451       | 0              |
| 3                  | 20                 | 0                       | 0.008288       | 0.001813       | 0              |
| 4                  | 12                 | 0                       | 0.135089       | 0.004562       | 0              |
| 4                  | 15                 | 0                       | 0.047898       | 0.001123       | 0              |
| 4                  | 20                 | 0                       | 0.014416       | 0.000163       | 0              |
| 4                  | 30                 | 0                       | 0.0329         | 0.000179       | 0              |
| 5                  | 15                 | 0                       | 0.032843       | 0.000978       | 0              |
| 5                  | 20                 | 0                       | 0.023417       | 5.08E-05       | 0              |
| 5                  | 30                 | 0                       | 0              | 0              | 0              |
| 8                  | 20                 | 0                       | 0              | 0              | 0              |
| 8                  | 30                 | 0                       | 0              | 0              | 0              |

Year

| weather window     |                    | polynomial coefficients |                |                |                |
|--------------------|--------------------|-------------------------|----------------|----------------|----------------|
| H <sub>s,max</sub> | V <sub>w,max</sub> | C <sub>0</sub>          | C <sub>1</sub> | C <sub>2</sub> | C <sub>3</sub> |
| 0.75               | 6                  | 82.60291                | 1.639936       | 0.246828       | 0.000772       |
| 0.75               | 8                  | 60.38231                | 5.063425       | -0.003153      | 0.001284       |
| 0.75               | 10                 | 64.74088                | 3.141411       | 0.07206        | 0.000418       |
| 1                  | 6                  | 39.90952                | 1.232015       | 0.179169       | 0              |
| 1                  | 8                  | 32.62395                | 2.203921       | 0.001876       | 0.000736       |
| 1                  | 10                 | 34.17694                | 1.307912       | 0.028422       | 0.000203       |
| 1                  | 12                 | 31.46166                | 1.60121        | 0.02087        | 0.000227       |
| 1.5                | 6                  | 23.0116                 | 0.799259       | 0.151157       | 0              |
| 1.5                | 8                  | 11.84377                | 1.38961        | 0.016352       | 0.000148       |
| 1.5                | 10                 | 13.78605                | 0.496921       | 0.008513       | 8.19E-05       |
| 1.5                | 12                 | 4.21224                 | 1.192668       | -0.000406      | 7.44E-05       |
| 2                  | 6                  | 14.65954                | 1.363067       | 0.144782       | 0              |
| 2                  | 8                  | 9.01333                 | 0.73863        | 0.018882       | 0.000139       |
| 2                  | 10                 | 3.806602                | 0.376982       | 0.010137       | 2.68E-05       |
| 2                  | 12                 | 0.438803                | 0.388704       | 0.006093       | 0              |
| 2                  | 15                 | 1.635813                | 0.266962       | 0.004782       | 0              |
| 3                  | 8                  | 4.886275                | 0.595197       | 0.03551        | 0              |
| 3                  | 10                 | 3.542891                | 0.262555       | 0.007979       | 2.94E-05       |
| 3                  | 12                 | 0                       | 0.222178       | 0.003489       | 0              |
| 3                  | 15                 | 0                       | 0.043883       | 0.000849       | 8.92E-06       |
| 3                  | 20                 | 0                       | 0.008134       | 0.001554       | 1.96E-06       |
| 4                  | 12                 | 0                       | 0.180522       | 0.004315       | 0              |
| 4                  | 15                 | 0                       | 0.037424       | 0.001387       | 0              |
| 4                  | 20                 | 0                       | 0.019252       | 0.00039        | 0              |
| 4                  | 30                 | 0                       | 0.038074       | -0.00025       | 5.26E-06       |
| 5                  | 15                 | 0                       | 0.021204       | 0.001261       | 0              |
| 5                  | 20                 | 0                       | 0.013826       | 7.31E-05       | 0              |
| 5                  | 30                 | 0                       | 0.022655       | 8.15E-05       | 0              |
| 8                  | 20                 | 0                       | 0.038705       | -0.00018       | 5.65E-07       |
| 8                  | 30                 | 0                       | 0              | 0              | 0              |